

# Large-Eddy Simulation of Marine Atmospheric Boundary Layers above a Spectrum of Moving Waves

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## ABSTRACT

Momentum and scalar transport in the marine atmospheric boundary layer (MABL) is driven by a turbulent mix of winds, buoyancy, and surface gravity waves. To investigate the interaction between these processes, a large-eddy simulation (LES) model is developed with the capability to impose a broadband spectrum of time-varying finite-amplitude surface waves at its lower boundary. The LES model adopts a Boussinesq flow model and integrates the governing equations on a time-varying, surface-fitted, nonorthogonal mesh using cell-centered variables with special attention paid to the solution of the pressure Poisson equation near the wavy boundary. Weakly unstable MABLs are simulated with geostrophic winds increasing from 5 to  $25 \text{ m s}^{-1}$  and wave age varying from swell-dominated to wind-wave equilibrium. The simulations illustrate cross-scale coupling as wave-impacted near-surface turbulence transitions into shear-convective rolls with increasing distance from the water. In a regime with swell, low winds, and weak heating, wave-induced vertical velocity and pressure signals are readily observed well above the standard reference height  $\zeta_a = 10 \text{ m}$ . At wind-wave equilibrium, the small-scale wave-induced signals are detectable only near the water surface. Below  $\zeta_a$ , a nearly-constant-flux layer is observed where the momentum flux carried by turbulence, form stress, and subgrid-scale motions shifts with varying wave age and distance above the water. The spectral content of the surface form stress is wave-age dependent, especially at low wavenumbers. The LES wind profiles deviate from Monin–Obukhov similarity theory in nonequilibrium wind-wave conditions, and entrainment is greatly enhanced by shear-induced engulfment events.

## 1. Introduction

To go beyond the current statistical description of atmosphere–wave–ocean coupling used in weather and climate models (e.g., [Chen et al. 2013](#); [Fan et al. 2012](#)) requires a deeper understanding of the coupling (or interaction) dynamics at time and space scales commensurate

with the winds, waves, and currents that exchange momentum and scalar fluxes in the lower atmosphere and upper ocean ([Sullivan and McWilliams 2010](#)). Numerous questions remain unsettled about wind-wave coupling processes in the marine atmospheric boundary layer (MABL); for example, the vertical extent of the wave-impacted (or wave induced) layer above the ocean surface, the role of swell, the validity of Monin–Obukhov (MO) similarity theory to predict surface fluxes, the correlation between winds and waves for varying wave state, and how wave-influenced surface wind and pressure fields blend into the bulk of the MABL, to mention just a few. Also there is still vigorous debate as to the mechanisms leading to wave growth, the role of critical layers ([Miles 1957](#); [Lighthill 1962](#); [Belcher and Hunt 1998](#);

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Hristov et al. 2003; Sajjadi et al. 2014), and the drag of the sea surface at high winds (Bell et al. 2012). Numerous field campaigns have provided important insights (e.g., Edson et al. 2007; Högström et al. 2009; Grare et al. 2013; Högström et al. 2013) but still lack some of the key observations (e.g., pressure–wave slope correlations), as they are forced to cope with the inherent unsteady motion of the wavy interface, the nonstationarity of wind-wave states, and the wide range of time and space scales involved [e.g., millimeters (spray) to kilometers (remotely generated swell)].

Turbulence-resolving direct numerical simulations (e.g., Sullivan et al. 2000; Yang and Shen 2010; Druzhinin et al. 2012; Richter and Sullivan 2013) and large-eddy simulations (Suzuki et al. 2013; Yang et al. 2013) of idealized wavy Couette flows along with recent laboratory measurements (e.g., Donelan et al. 2004; Veron et al. 2007) have added to the understanding of wind-wave couplings. For example, this body of work highlights the importance of wave age in generating wave-induced motions and the impact of wave breaking, flow separation, and wind speed on surface drag. However, large-scale turbulence generated by shear and convection, three-dimensional boundary layer winds generated by rotation, and a broadband spectrum of surface waves, which are fundamental to the MABL, are of course missing in these small-scale studies.

High Reynolds number large-eddy simulation (LES) has the potential to shed light on wind-wave coupling processes in the MABL, but its application is relatively unexplored because of the complexity of including a time-evolving wave field with multiple modes and the high computational expense required to span a wide range of scales. The topic of the present paper is the latter (i.e., to develop and apply LES to a realistic stratified MABL where the lower boundary is a resolved spectrum of time-dependent surface gravity waves). The computational method described here allows for nearly arbitrary 3D wave fields [i.e., the sea surface elevation  $h = h(x, y, t)$  is a surface boundary condition;  $h(x, y, t)$  is assumed to be a single-valued function]. The spatial scales of the resolved turbulence and waves considered are on the order of meters up to the height of the MABL  $z_i \sim O(500 \text{ m})$  or more. Covering this broad range of scales requires a large number of mesh points and significant computational power. In the current problem posing, the surface waves are externally imposed based on existing empirical wave spectra with the assumption of a linear-mode random-phase model for the wave amplitudes. The missing phase information can in principle be obtained by using advanced observational techniques of the sea surface (Romero and Melville 2010). The present work continues past efforts that

coupled the MABL with an idealized single monochromatic wave (Sullivan et al. 2008; Nilsson et al. 2012), but it is a significant advance over these earlier developments.

The outline of the paper is as follows: section 2 is an introduction to the LES equations appropriate for a high Reynolds number atmospheric boundary layer and their transformation to time-dependent curvilinear coordinates, section 3 outlines the numerical method, section 4 describes results for a weakly unstable MABL with varying geostrophic winds, and section 5 provides a summary of the current findings.

## 2. Governing equations

In the description of the model equations, given below, the following notation is used:  $u_i = (u, v, w)$  denotes the Cartesian velocity components,  $\theta$  is virtual potential temperature,  $p^*$  is the pressure variable normalized by density  $\rho$ , and  $e$  is the subgrid-scale (SGS) energy. Flow variables ( $u_i, \theta, p^*, e$ ) are interpreted as LES spatially filtered quantities.

### a. Atmospheric LES model equations

The set of spatially filtered LES equations applicable to turbulent flow in the atmospheric boundary layer under the Boussinesq assumption is (e.g., Moeng 1984; McWilliams et al. 1999)

$$\frac{\partial u_i}{\partial x_i} = 0, \quad (1a)$$

$$\begin{aligned} \frac{\partial u_i}{\partial t} = & -\frac{\partial u_j u_i}{\partial x_j} - \frac{\partial p^*}{\partial x_i} - 2\epsilon_{ijk} \Omega_j u_k \\ & + \delta_{i3} \beta (\theta - \theta_o) - \frac{\partial \tau_{ij}}{\partial x_j} - \frac{\partial \mathcal{P}}{\partial x_i}, \end{aligned} \quad (1b)$$

$$\frac{\partial \theta}{\partial t} = -\frac{\partial u_i \theta}{\partial x_i} - \frac{\partial \tau_{i\theta}}{\partial x_i}, \quad (1c)$$

$$\frac{\partial e}{\partial t} = -\frac{\partial u_i e}{\partial x_i} - \tau_{ij} S_{ij} + \beta \tau_{3\theta} + \frac{\partial}{\partial x_j} \left( 2\nu_t \frac{\partial e}{\partial x_j} \right) - \mathcal{E}. \quad (1d)$$

In the above,  $\Omega_i = (0, 0, \Omega \sin \Phi)$ , with Earth's rotation and latitude denoted  $\Omega$  and  $\Phi$ , respectively; the buoyancy parameter  $\beta = g/\theta_o$ , where the gravitational acceleration is  $g$  and the reference (still air) virtual potential temperature is  $\theta_o$ ; and the large-scale external pressure gradients normalized by density  $\partial \mathcal{P}/\partial x_i$  drive the boundary layer winds. A Boussinesq flow model requires that  $p^*$ , the pressure variable, be determined

from an elliptic Poisson pressure equation to enforce mass conservation (see [section 3d](#)). Ultimately, the SGS momentum and temperature (or scalar) fluxes ( $\tau_{ij}$ ,  $\tau_{i\theta}$ ), respectively, require modeling in the interior of the flow and at the lower boundary (see [section 3f](#)) to close the system of equations. In the SGS turbulence kinetic energy (TKE) equation [see (1d)], the time evolution of  $e$  depends on right-hand-side terms (in order): advection by the resolved field, energy transfer between resolved and SGS motions where the resolved scale strain rate  $S_{ij} = (1/2)(\partial u_i/\partial x_j + \partial u_j/\partial x_i)$ , SGS buoyancy flux, Laplacian diffusion with turbulent eddy viscosity  $\nu_t$ , and viscous dissipation  $\mathcal{E}$ . Molecular diffusion terms are neglected assuming that the molecular Reynolds number is high. A discussion of the modeling of the SGS fluxes is postponed until [section 2d](#).

### b. Coordinate transformation

We adapt our LES model with a flat boundary ([Sullivan and Patton 2011](#)) to the situation with a three-dimensional time-dependent lower boundary with shape  $h = h(x, y, t)$  by applying a transformation to the physical space coordinates  $x_i \equiv (x, y, z)$  that maps them onto computational coordinates  $\xi_i \equiv (\xi, \eta, \zeta)$ . The computational mesh in physical space is surface following, non-orthogonal, and time varying. Vertical gridlines are held fixed at a particular  $(x, y)$  location on the surface but translate vertically as a function of time  $t$ . A transformation that obeys these constraints and maps the physical domain to a flat computational domain  $x_i \Rightarrow \xi_i$  is the rule:

$$\begin{aligned} \tau &= t, & \xi &= \xi(x) = x, \\ \eta &= \eta(y) = y, & \zeta &= \zeta(t, x, y, z). \end{aligned} \quad (2)$$

The differential metrics  $\partial x_i/\partial \xi_j$  and  $\partial \xi_i/\partial x_j$ , which are needed in formulating the LES model in curvilinear coordinates, are connected through the mapping transformation. This can be done for general transformations (e.g., [Anderson et al. 1984](#), 252–253), but here we take advantage of the simplified terrain-following grid in (2). This leads to the reduced set of nonzero metric relationships:

$$\begin{aligned} \zeta_t &= -z_t J, & \xi_x &= \eta_y = 1, & \zeta_x &= -z_\xi J, \\ \zeta_y &= -z_\eta J, & \zeta_z &= 1/z_\zeta J, \end{aligned} \quad (3)$$

where  $J$  is the Jacobian and subscripts denote partial differentiation. The time dependence of the mapping appears in (3), where  $\partial z/\partial t = z_t$  is the grid speed (i.e., the vertical velocity of individual grid points). We define the rule in (2) that maps physical space onto flat

computational space at any time by the following prescription:

$$z = \zeta + h(x, y, t) \left(1 - \frac{\zeta}{Z_L}\right)^\varpi, \quad (4)$$

where  $Z_L$  is the top of the computational domain and  $\varpi$  controls how rapidly the horizontal gridlines become level surfaces in physical space. Typically we use  $\varpi = 3$ , which vertically squeezes (stretches) near-surface grid cells at the wave crests (troughs) by a modest amount, approximately 20%. For  $\varpi = 1$ , (4) reduces to  $\zeta = (z - h)/(1 - h/Z_L)$ , which is commonly used to map stationary terrain onto flat computational coordinates (e.g., [Henn and Sykes 1999](#)). Equation (4) is a single-valued mapping that produces smooth continuous metric derivatives ( $\partial \xi_i/\partial x_j$ ,  $\partial \xi_i/\partial t$ ) in the interior of the computational domain depending on the smoothness of the boundary shape derivatives ( $h_t, h_x, h_y$ ).

### c. LES equations in time-dependent curvilinear coordinates

The transformation of the LES equations to curvilinear coordinates is obtained by applying the chain rule for differentiation and making frequent use of the metric identity (e.g., [Anderson et al. 1984](#), p. 254):

$$\frac{\partial}{\partial \xi_j} \left( \frac{1}{J} \frac{\partial \xi_j}{\partial x_i} \right) = 0. \quad (5)$$

To cast the equations in fully conservative form, however, requires care in treating the time derivative. For example, the time derivative of density transforms as

$$\frac{\partial \rho}{\partial t} \Big|_{\mathbf{x}} = J \left[ \frac{\partial}{\partial t} \left( \frac{\rho}{J} \right) + \frac{\partial}{\partial \xi_i} \left( \frac{\rho}{J} \frac{\partial \xi_i}{\partial t} \right) \right]_{\xi} = 0, \quad (6)$$

provided the grid movement obeys

$$\frac{\partial}{\partial t} \left( \frac{1}{J} \right) + \frac{\partial}{\partial \xi_i} \left( \frac{1}{J} \frac{\partial \xi_i}{\partial t} \right) = 0. \quad (7)$$

Equation (7) is a restatement of the so-called geometric (or space) conservation law (GCL) and should be satisfied by the numerical discretization in order for the scheme to be conservative ([Thomas and Lombard 1979](#); [Demirdžić and Perić 1990](#)).<sup>1</sup> For our surface following

<sup>1</sup> [Thomas and Lombard \(1979, p. 1032\)](#) develop the geometric conservation law using an integral formulation but note that it can equally be derived from the differential form of the governing equations by setting  $\rho = 1$  and  $u_i = 0$ , which is the procedure used here.

grid the GCL simply reduces to (8b) since  $\partial\xi_i/\partial t = (0, 0, -z_t J)$ . Section 3c describes how (7) is used to track the motion of the grid.

The complete set of LES equations in computational coordinates under the time-dependent surface-following transformation (2) and (3) is then

$$\frac{\partial U_i}{\partial \xi_i} = 0, \quad (8a)$$

$$\frac{\partial}{\partial t} \left( \frac{1}{J} \right) - \frac{\partial z_t}{\partial \zeta} = 0, \quad (8b)$$

$$\frac{\partial}{\partial t} \left( \frac{u_i}{J} \right) + \frac{\partial}{\partial \xi_j} [(U_j - \delta_{3j} z_t) u_i] = \frac{\mathcal{F}_i}{J}, \quad (8c)$$

$$\frac{\partial}{\partial t} \left( \frac{\theta}{J} \right) + \frac{\partial}{\partial \xi_j} [(U_j - \delta_{3j} z_t) \theta] = \frac{\mathcal{M}}{J}, \quad (8d)$$

$$\frac{\partial}{\partial t} \left( \frac{e}{J} \right) + \frac{\partial}{\partial \xi_j} [(U_j - \delta_{3j} z_t) e] = \frac{\mathcal{R}}{J}, \quad (8e)$$

$$\frac{\partial}{\partial \xi_i} \left( \frac{1}{J} \frac{\partial \xi_i}{\partial x_j} \frac{\partial \xi_m}{\partial x_j} \frac{\partial p^*}{\partial \xi_m} \right) = \mathcal{S}, \quad (8f)$$

where (8a) is the mass conservation (continuity) equation, (8c) is the momentum transport equation, (8d) is the transport equation for potential temperature, (8e) is the subgrid-scale energy transport equation, and (8f) is the pressure Poisson equation. The right-hand sides of (8c)–(8e) model physical processes in the atmospheric boundary layer, namely, pressure gradients, Coriolis rotation, divergence of subgrid-scale fluxes, buoyancy, and, in the case of the SGS  $e$  equation, also turbulent diffusion and viscous dissipation. For completeness these terms are gathered here:

$$\begin{aligned} \frac{\mathcal{F}_i}{J} = & -\frac{\partial}{\partial \xi_j} \left( \frac{p^*}{J} \frac{\partial \xi_j}{\partial x_i} \right) + \delta_{3i} \frac{g}{J \theta_o} (\theta - \theta_o) \\ & - \frac{\partial}{\partial \xi_j} \left( \frac{\tau_{ik}}{J} \frac{\partial \xi_j}{\partial x_k} \right) - 2\epsilon_{ijk} \Omega_j \frac{u_k}{J} - \frac{1}{J} \frac{\partial \mathcal{P}}{\partial x_i}, \end{aligned} \quad (9a)$$

$$\frac{\mathcal{M}}{J} = -\frac{\partial}{\partial \xi_j} \left( \frac{\tau_{i\theta}}{J} \frac{\partial \xi_j}{\partial x_i} \right), \quad (9b)$$

$$\frac{\mathcal{R}}{J} = -\frac{\tau_{ij} S_{ij}}{J} + \frac{\beta \tau_{3\theta}}{J} + \frac{\partial}{\partial \xi_j} \left( \frac{2\nu_t}{J} \frac{\partial e}{\partial \xi_m} \frac{\partial \xi_m}{\partial x_k} \frac{\partial \xi_j}{\partial x_k} \right) - \frac{\mathcal{E}}{J}. \quad (9c)$$

Momentum and scalar advection are compactly written in strong flux-conservation form using the volume flux or “contravariant flux” velocity:

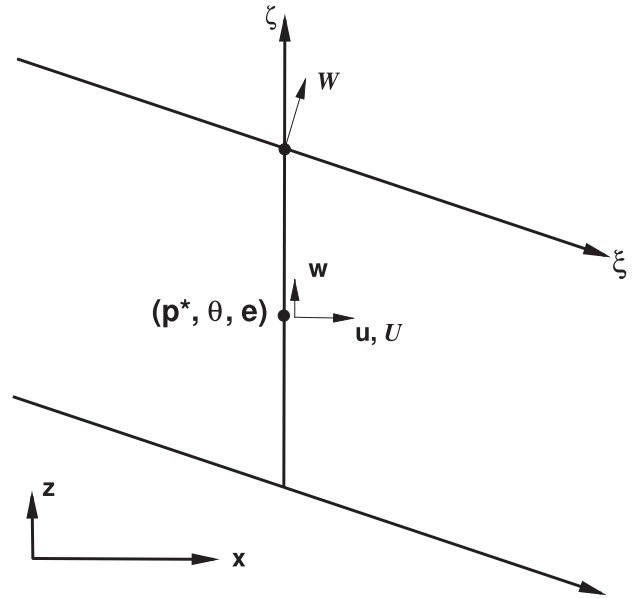


FIG. 1. A two-dimensional sketch illustrating the layout of the cell-centered Cartesian velocity components ( $u, w$ ), along with the pressure  $p^*$ , potential temperature  $\theta$ , and SGS energy  $e$ . The contravariant flux velocity  $W$  is located at a cell face and is oriented perpendicular to a constant- $\zeta$  surface. The contravariant flux velocity  $U$  is oriented perpendicular to a constant- $\xi$  surface and is also located at a cell center (see section 3a). The horizontal velocity components  $v$  and  $V$ , which are not shown, point into the page at the cell center.

$$U_i = \frac{u_j}{J} \frac{\partial \xi_i}{\partial x_j}, \quad (10)$$

where  $U_i = (U, V, W)$  are normal to a surface of constant  $\xi_i$  (see Fig. 1).

The time dependence of the grid modifies the LES equations: the Jacobian appears inside the time tendency of each transport equation and, as anticipated, the total vertical flux of a variable  $\psi$  depends on the difference between the contravariant flux velocity and the grid speed  $(W - z_t)\psi$ . Examination of (8) shows that if the velocity and scalar fields are set to constant values then the left-hand sides of (8c)–(8e) reduce to (8b). Hence, the numerical method needs to satisfy the reduced form of the GCL discretely in order to prevent artificial sources and sinks from developing in the computational domain (see section 3c).

#### d. Parameterization of SGS motions

Formally, the LES equations are obtained by applying a spatial filter to the full governing equations (e.g., Wyngaard 2004). The filter is assumed to be homogeneous in space and time, and, as a result, the operation order of differentiation and filtering can be interchanged.

For boundary layer flows, this assumption is violated and a commutation error occurs near walls (Ghosal and Moin 1995), but the error is almost always ignored in LES implementations as the inaccuracies in SGS wall modeling are viewed as of greater importance (Sullivan et al. 2003). The parameterization problem is even more pronounced with a multimode moving lower boundary because of filtered products of fluctuating metric coefficients and velocity (Chalikov 1978), and extra stresslike terms arise from filtering the boundary shape (Nakayama et al. 2009). In the present application, the flow is assumed to be laterally periodic and our wave-following grid transformation results in  $x = \xi$  and  $y = \eta$ . Thus, we adopt the simplest approach and employ the filtering operation and standard SGS models as in our flat LES code but account for the varying filter width. The LES equations are closed using the SGS parameterizations outlined by Deardorff (1972) and analyzed by Moeng and Wyngaard (1988). Also, the solutions are explicitly filtered (i.e., dealiased) in  $\xi$ - $\eta$  planes at the end of each time step. This parameterization utilizes an eddy viscosity for SGS momentum and temperature fluxes, and the Lilly–Kolmogorov model for viscous dissipation:

$$\tau_{ij} = -2\nu_t S_{ij}, \quad \tau_{i\theta} = -\nu_h \frac{\partial \theta}{\partial x_i}, \quad \mathcal{E} = C_\varepsilon \frac{e^{3/2}}{\Delta}. \quad (11)$$

The turbulent eddy viscosity  $\nu_t = C_k \Delta \sqrt{e}$  and turbulent diffusivity  $\nu_h = (1 + 2\ell/\Delta)\nu_t$  evolve under the action of the transport equation for SGS TKE [see (8e)]. The constants  $(C_k, C_\varepsilon) = (0.1, 0.93)$  and corrections to the stability corrected length scale  $\ell$  are found in Moeng (1984) and Moeng and Wyngaard (1988). The filter length scale  $\Delta$  is computed from the averaging volume  $\Delta^3 = (3/2)^2(\Delta\xi\Delta\eta\Delta\zeta/J)$  with the  $3/2$  factor accounting for dealiasing. Because of movement and the stretching–squeezing of vertical gridlines,  $\Delta$  varies with position and time. To reduce the reliance on the SGS model, we use fine resolution near the surface (see section 4a). Since the large wave motions are fully resolved, the total TKE at the surface is often large and dominated by resolved variances, further reducing the impact of the SGS model compared to a situation with flat stationary walls.

#### e. Wave field prescription

To complete our LES model for the MABL, we need to prescribe the height of the surface wave field  $h(x, y, t)$  in physical space over a typical horizontal domain of the LES. In the absence of a full description of the wave field kinematics and phase relationships, we adopt simplifications that allow us to use existing

information. Time and space maps of  $h(x, y, t)$  are constructed based on typical empirical fits of measured two-dimensional wave spectra:

$$E(k, \phi) = S(k)D(k, \phi), \quad (12)$$

where the amplitude  $S(k)$  and directional  $D(k, \phi)$  spectra depend on the magnitude of the horizontal wavenumber  $k = |\mathbf{k}| = |k_x \hat{\mathbf{i}} + k_y \hat{\mathbf{j}}|$  and wave direction  $\phi$ . We choose the functional forms for  $S(k)$  and  $D(k, \phi)$  proposed by Donelan et al. (1985) [see also p. 187 of Komen et al. (1994)], which depend on bulk environmental parameters, namely, the reference average surface wind speed  $U_a$  at  $\zeta_a = 10$  m, the phase speed of the peak in the wave height spectrum  $C_p$ , their ratio (the wave age)  $C_p/U_a$ , and the mean wave propagation direction  $\langle \phi \rangle$ . To use these measured spectra, which are expressed in terms of radial frequency  $\omega$ , in the LES they are transformed into wavenumber space using the linear dispersion relation  $|\mathbf{k}| = \omega^2/g$  and properly weighted such that the resulting wavenumber spectra are variance preserving (Phillips 1977, p. 105). In physical space, the rule for constructing the synthetic wave field  $h(x, y, t)$  is as a sum of linear plane waves, each with random phase  $\varphi$ :

$$h(\mathbf{x}, t) = \sum_{\mathbf{k}} A(k) \exp\{i[\mathbf{k} \cdot \mathbf{x} - \omega(k)t + \varphi]\}, \quad (13)$$

where the amplitude  $A^2(k) = S(k)D(k, \phi)dk_x dk_y$ . The random phase model in (13) is computationally advantageous since only an initial wave state  $h(x, y, t_0)$  is required and it also easily adapts to the horizontal dimensions of the LES domain. Two-dimensional fast Fourier transforms (FFTs) are used to compute future values of  $h(x, y, t)$  as well as the time and space derivatives of the boundary shape  $(h_t, h_x, h_y)$ , which are needed to construct the moving mesh and the surface boundary conditions.

#### f. Velocity boundary condition

Both the wind and wave fields are assumed to be spatially periodic in computational  $\xi$ - $\eta$  planes and at  $\zeta = 0$  a boundary condition on the winds is imposed consistent with the surface wave field. The total time rate of change of the wave height is

$$\frac{dh}{dt} = w_o = h_t + u_o h_x + v_o h_y, \quad (14)$$

where  $(u_o, v_o, w_o)$  are the water motions. Initially, we assume these water motions are dominated by the wave orbital velocities [i.e., there is no net current; see discussion by Banner and Melville (1976) and Banner (1990)].



The contravariant velocity component normal to the water surface is given by (10):

$$W = u \frac{\zeta_x}{J} + v \frac{\zeta_y}{J} + w. \quad (15)$$

Matching (14) and (15) and requiring no flow normal to (across) the wavy boundary leads to

$$W - h_t = 0 \quad \text{at} \quad \zeta = 0. \quad (16)$$

Equation (16) effectively implies that spray and bubbles do not pass through the interface in our problem. At the upper boundary of the computational domain, the horizontal gridlines are level surfaces in physical space with  $z_{\xi} = z_{\eta} = 0$ . Then

$$W = w = z_t \quad \text{at} \quad \zeta = Z_L, \quad (17)$$

so that the resolved vertical flux of momentum and scalars is zero across the top boundary. The specification of the surface fluxes appropriate for a high Reynolds number rough-wall LES model taking into account the wave motion is described in section 3f.

### 3. Numerical method

#### a. Spatial discretization and variable layout

The LES set of (8a)–(8e) is discretized using the well-developed techniques in our flat bottom boundary codes (Moeng 1984; Sullivan et al. 1996). Spatial derivatives in the  $(\xi, \eta)$  computational coordinates are estimated using pseudospectral approximations while centered second-order-accurate finite-difference approximations are employed for  $\zeta$  derivatives. To be compliant with (8b), the spatial differencing evaluates the advective terms in (8c)–(8e) in flux form as opposed to the rotational form used by Moeng (1984) or skew-symmetric form used by Sullivan et al. (2000). The variable layout in the computational mesh uses a collocated arrangement for the fundamental solution variables  $(u_i, p^*, \theta, e)$ , which is advantageous as it results in a compact differencing stencil and is also applicable to meshes with large bends in the coordinate lines (Zang et al. 1994; Sullivan et al. 2000). The fundamental difficulty of tightly coupling the velocity and pressure in a collocated mesh is circumvented by locating the contravariant flux velocities at cell faces mimicking the usual arrangement in a staggered mesh as shown in Fig. 1.

#### b. Time advancement

Time integration is a fully explicit third-order Runge–Kutta (RK3) scheme (Spalart et al. 1991; Sullivan et al.

1996, 2008) that uses dynamic time stepping with a fixed Courant–Friedrichs–Lewy (CFL) number and employs a fractional step method to enforce the divergence-free condition. The general rule for advancing a cell-centered Cartesian velocity variable to a new time level  $n$  over a time step  $\Delta t$  is

$$\frac{u_i}{J} \Big|_n = \frac{\hat{u}_i}{J} \Big|^{n-1} - \Delta t \alpha_n \frac{\partial}{\partial \xi_j} \left( \frac{p^*}{J} \frac{\partial \xi_j}{\partial x_i} \right)^n, \quad (18)$$

where the pressure gradient is written in conservative form. The intermediate velocity

$$\frac{\hat{u}_i}{J} \Big|^{n-1} = \frac{u_i}{J} \Big|^{n-1} + \Delta t \alpha_n \frac{q_i}{J} \Big|^{n-1} + \Delta t \beta_n \frac{Q_i}{J} \Big|^{n-2} \quad (19)$$

is the discrete sum of the full right-hand-side  $Q_i/J$  from the previous time (or stage) step  $(n-2)$  and the partial right-hand-side  $q_i/J$  from the current time  $(n-1)$  minus the pressure contributions;  $\alpha_n$  and  $\beta_n$  are weights associated with the RK3 scheme (Sullivan et al. 2000). The time integration rule for scalar fields is identical to (18) and (19) in the absence of pressure gradients. The divergence-free condition is satisfied at every RK3 stage, as opposed to the method advocated by Le and Moin (1991) (see also Zheng and Petzold 2006), which projects the velocity onto a divergence-free field only at the final stage. The latter scheme is computationally more efficient since it reduces pressure iterations over a full time step, but both flux and skew-symmetric forms of the advection term in our scalar equations are based on satisfying (8a) at all stages of the RK3 time advancement. Attempts to use the method of Le and Moin (1991) resulted in numerical instabilities.

#### c. Geometric conservation law

The geometric conservation law [(8b)] is satisfied using the same time-advancement scheme as for velocity and scalar fields [see (18)]. Given an externally imposed wave field,  $h(x, y, t)$  is known at current and future time steps  $(n-1, n)$  and we can then construct the distribution of vertical grid points at “ $W$  points,” [viz.,  $z(x, y)^{(n-1, n)}$  according to the map of (4)]. Jacobians  $J^{(n-1, n)}$  are then naturally built from the transformation rule in (3). Since we choose to specify the grid point locations at future time steps, we then find matching grid speeds  $z_t(x, y)$  so that (8b) is obeyed discretely. The companion to (18), appropriately inverted, for determining grid speeds is the semidiscrete relationship:

$$\frac{\partial z_t}{\partial \zeta} \Big|^{n-1} = \frac{1}{\alpha_n \Delta t} \left[ \frac{1}{J} \Big|_n - \frac{1}{J} \Big|^{n-1} - \Delta t \beta_n \left( \frac{\partial z_t}{\partial \zeta} \right)^{n-2} \right]. \quad (20)$$

This first-order equation is integrated vertically from the surface to the top of the domain with the boundary condition  $z_t = h_t$  at  $\zeta = 0$ . We emphasize that the upper boundary of our computational domain is far from the lower surface and the wave-following gridlines in the interior of the domain quickly asymptotically approach flat level surfaces with increasing  $\zeta$ . As a result,  $z_t$  at a particular  $x$ - $y$  grid point must vary with distance from the wave surface. This is different than the scheme proposed by Chalikov (1998) in which the grid speeds at all  $\zeta$  are equal to the vertical motion of the wave field (i.e.,  $z_t$  is constant with height). The latter scheme also implies that the computational mesh at any  $\zeta$ , including the upper boundary, mimics the shape of the lower surface, which complicates posing upper boundary conditions. There is a subtlety in the implementation of (20). Since our time stepping is explicit, the value of  $z_t$  diagnosed from (20) is at time level  $n - 1$  but uses gridpoint locations at time level  $n$ . In other words, if the wave field is imposed, diagnosing the grid speed at time  $n$  requires knowledge about the wave shape at a future time  $n + 1$ . The end result is that the grid must be stored at three time levels in the LES code. Information about the wave field at each RK3 stage is used in two ways in the grid generation:  $h(x, y, t)$  is used to position the grid nodes in the mesh and  $h_t(x, y, t)$  is used to determine how rapidly the grid nodes in the mesh move to their new locations.

#### d. Pressure Poisson equation

The heart of the numerical scheme is the formulation and solution of a pressure Poisson equation that results in a flow field consistent with our incompressible Bousinesq flow model. As is standard practice, we develop a pressure equation by combining the continuity equation and our time-stepping scheme. Substitution of (18) into (10) leads to the time advance rule for the contravariant velocity:

$$U_i^n = \hat{U}_i^{n-1} - \frac{\Delta t \alpha_n}{J} \frac{\partial \xi_i}{\partial x_j} \frac{\partial \xi_m}{\partial x_j} \frac{\partial p^*}{\partial \xi_m} \Big|^{n-1}, \quad (21)$$

where now the pressure gradient is expanded in non-conservative form. Momentum interpolation (Sullivan et al. 2000) of the Cartesian velocity components is used to build

$$\hat{U}_i = \frac{\hat{u}_j}{J} \Big|_I \frac{\partial \xi_i}{\partial x_j}, \quad (22)$$

where  $(\cdot)|_I$  denotes an interpolated value. As mentioned previously, because of the spatial differencing scheme,

only  $\hat{W}|^{n-1}$ , located at the upper and lower cell faces, requires interpolation (see section 3a). The divergence of (21) leads to the pressure Poisson equation:

$$\frac{\partial}{\partial \xi_i} \left( \frac{1}{J} \frac{\partial \xi_i}{\partial x_j} \frac{\partial \xi_m}{\partial x_j} \frac{\partial p^*}{\partial \xi_m} \right)^n = \frac{1}{\Delta t \alpha_n} \frac{\partial \hat{U}_i}{\partial \xi_i} \Big|^{n-1}. \quad (23)$$

Our strategy for finding the pressure utilizes an iterative method that avoids directly forming the complicated left-hand side of (23). Instead, examination of (18), (21), and (23) suggests the equivalent stationary iteration scheme to find  $p^{*,n}$ :

$$\mathcal{L}(p^{*,i+1}) = \mathcal{L}(p^{*,i}) - \frac{1}{\Delta t \alpha_n} \frac{\partial U_k(p^{*,i})}{\partial \xi_k}, \quad (24)$$

where the source term is the divergence-free condition, superscript  $i$  denotes the iteration index, and the linear preconditioning operator is

$$\mathcal{L}(p^*) = \frac{1}{\langle J \rangle} \left( \frac{\partial^2 p^*}{\partial \xi^2} + \frac{\partial^2 p^*}{\partial \eta^2} \right) + \frac{\partial}{\partial \zeta} \left( \langle J \rangle \frac{\partial p^*}{\partial \zeta} \right). \quad (25)$$

At each iteration, we update  $U_k$  using the latest  $p^{*,i}$  field according to (21) and then compute the new right-hand side of (24). The operator  $\mathcal{L}$  is an easily invertible diagonal approximation of the left-hand side of (23) with the spatially averaged Jacobian

$$\langle J \rangle(\zeta) = \int_{\eta} \int_{\xi} J(\xi, \eta, \zeta) d\xi d\eta. \quad (26)$$

Equation (24) is solved using standard methods, namely, 2D Fourier decomposition in  $\xi$ - $\eta$  planes followed by tridiagonal matrix inversion in the  $\zeta$  direction. Inversion of (24) is expensive because its computational steps require global communication in a parallel algorithm (Sullivan and Patton 2011). The iterative solution for pressure in the presence of wavy boundaries increases the overall computational cost of simulations by approximately 50% compared to simulations with flat lower boundaries where the pressure is solved for directly.

#### e. Pressure boundary conditions at a wavy boundary

Compatible velocity and pressure boundary conditions are naturally built into the iteration scheme given by (24). First, the proper surface boundary condition on the diagonal preconditioner  $\mathcal{L}$  is simply  $\partial p^*/\partial \zeta = 0$ , which is the condition applied in a flat-wall LES with a Cartesian grid. The proper pressure boundary condition used in the source term  $\partial U_k(p^*)/\partial \xi_k$  of (24),

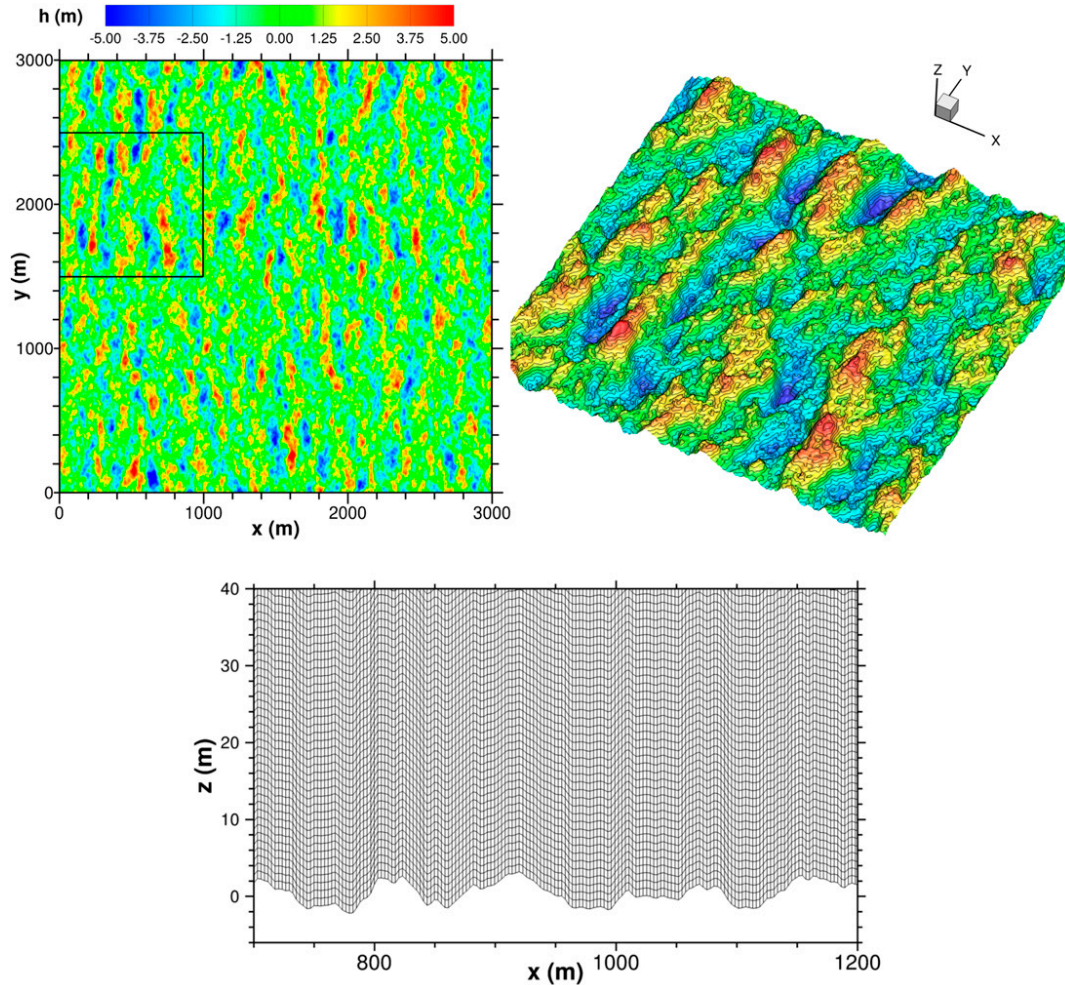


FIG. 2. A snapshot of the wave field height  $h(x, y, t)$  that is imposed at the bottom of the LES. (top left) Depiction of  $h(x, y, t)$  over the entire horizontal domain  $3000 \times 3000 \text{ m}^2$ . (top right) A 3D blowup of the  $1 \times 1 \text{ km}^2$  area blocked off by the black line in the top-left panel; illustrates the multiscale nature of the wave field. (bottom) The instantaneous grid on an  $x$ - $z$  plane in the lowest portion of the MABL that conforms (i.e., surface fitted) to  $h(x, y, t)$ . For clarity, only a small fraction of the grid is displayed.

however, needs to account for the nonorthogonal mesh [also see Zang et al. (1994), p. 22]. This boundary condition is exposed by examining the update for  $(U, V, W)$  in advancing time from  $n - 1$  to  $n$  given by (21):

$$U|_n = \hat{U}|^{n-1} - \Delta t \alpha_n \left( \frac{1}{J} \frac{\partial p^*}{\partial \xi} + \frac{\zeta_x}{J} \frac{\partial p^*}{\partial \zeta} \right)^n, \quad (27a)$$

$$V|_n = \hat{V}|^{n-1} - \Delta t \alpha_n \left( \frac{1}{J} \frac{\partial p^*}{\partial \eta} + \frac{\zeta_y}{J} \frac{\partial p^*}{\partial \zeta} \right)^n, \quad (27b)$$

$$W|_n = \hat{W}|^{n-1} - \Delta t \alpha_n \left( \frac{\zeta_x^2 + \zeta_y^2 + \zeta_z^2}{J} \frac{\partial p^*}{\partial \zeta} + \frac{\zeta_x}{J} \frac{\partial p^*}{\partial \xi} + \frac{\zeta_y}{J} \frac{\partial p^*}{\partial \eta} \right)^n. \quad (27c)$$

In the interior of the computational domain, the pressure gradient  $\partial p^*/\partial \zeta$ , which appears in all three equations, is evaluated using standard second-order centered finite-difference formulas, while the pressure gradients  $\partial p^*/\partial \xi$  and  $\partial p^*/\partial \eta$  are evaluated using pseudospectral differencing. Inspection of (27a) and (27b) shows that updating  $U$  and  $V$  using a centered formula for  $\partial p^*/\partial \zeta$  at the first level  $\zeta = \Delta \zeta/2$  above the wavy boundary requires the pressure field at  $\zeta = 3\Delta \zeta/2$  and at the ghost point  $\zeta = -\Delta \zeta/2$  below the wavy boundary. Along  $\zeta = -\Delta \zeta/2$ ,  $U$  and  $V$  are globally connected to an entire plane of ghost-point pressures  $p^*(x, y, -\Delta \zeta/2)$  through the gradients  $\partial p^*/\partial \xi$  and  $\partial p^*/\partial \eta$ .

To find the proper ghost-point pressures, we use the  $W$  equation, its surface boundary condition, and



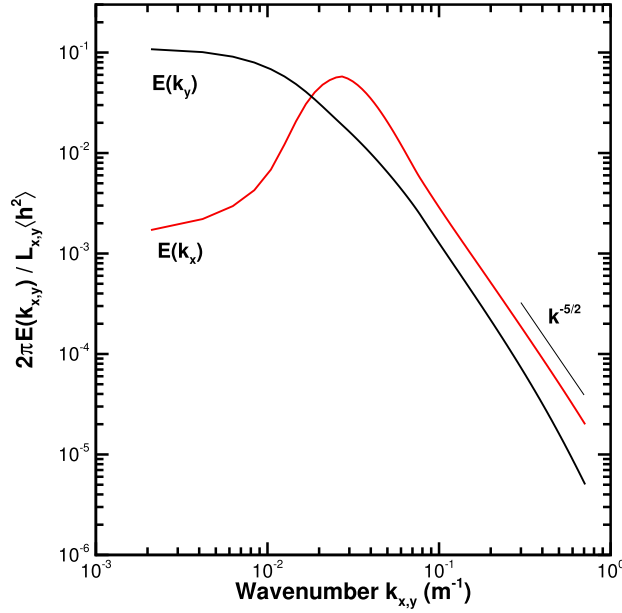


FIG. 3. The 1D spectra of the wave height as function of the horizontal wavenumber  $k_x$  or  $k_y$ . Both  $E(k_x)$  and  $E(k_y)$  are normalized by the wave height variance  $\langle h^2 \rangle$ . The wave fields here and in Fig. 2 are generated assuming wind-wave equilibrium  $C_p/U_a = 1.2$  with a surface wind speed  $U_a = 15 \text{ m s}^{-1}$ .

our iteration scheme. At  $\zeta = 0$ , (27c) is rearranged to yield

$$\left[ \frac{\zeta_x^2 + \zeta_y^2 + \zeta_z^2}{J} \frac{p^*(\xi, \eta, \Delta\zeta/2) - p^*(\xi, \eta, -\Delta\zeta/2)}{\Delta\zeta} \right]^i = \frac{\hat{W} - h_t}{\Delta t \alpha_n} - \left( \frac{\zeta_x}{J} \frac{\partial p^*}{\partial \xi} + \frac{\zeta_y}{J} \frac{\partial p^*}{\partial \eta} \right)^{i-1}, \quad (28)$$

where we impose the boundary condition (16). The superscript  $i$  in (28) is again the iteration index, and for clarity we drop the superscripts  $n$  and  $n-1$  denoting the time step. At each iteration with a known field  $p^*(\xi, \eta, \Delta\zeta/2)^i$ , (28) is rearranged to solve for the ghost-point

pressure  $p^*(\xi, \eta, -\Delta\zeta/2)^i$  with the right-hand side (centered on  $\zeta = 0$ ) lagged from the previous iteration. Subsequently, (27a) and (27b) are updated at all interior nodes and a pressure iteration is completed by sweeping through (24) with a new right-hand side. The term  $\hat{W}(\zeta = 0)$ , which appears in (28), is constant during pressure iterations and is obtained from interior-node interpolations.

#### f. Surface fluxes

In high winds, the ocean surface is assumed to be in a fully rough regime with negligible contributions from the thin molecular viscous sublayer (Donelan 1998). Here, we follow the approach of second-order closure modeling for turbulent flow over hills and waves and assume that the water surface is fully rough so that the surface fluxes of momentum and scalars can be represented in terms of law-of-the-wall relationships (e.g., Gent and Taylor 1976; Makin et al. 1995; Belcher and Hunt 1998). This approach is less certain in LES modeling where surface undulations (or waves) are partially resolved; that is, the velocity and pressure fields induced by the large energetic components of the wave field are resolved and the smaller-scale, less-energetic waves are unresolved (e.g., Nakayama et al. 2004; Yang et al. 2013). We simply parameterize the effects of the unresolved waves (i.e., those below the cutoff scale of the LES), using a bulk  $z_o$  roughness. Then the bulk aerodynamic formulas are applied point by point along the wave boundary with this imposed  $z_o$  roughness to compute the surface momentum and scalar fluxes as described in the appendix.

## 4. Turbulent winds over waves

### a. Simulation details

The parameter space spanned by the many combinations of large-scale winds, surface heating, and surface waves forcing an MABL is extremely broad and can

TABLE 1. Simulation properties:  $U_g$  is the geostrophic wind;  $C_p/U_a$  is wave age;  $U_a$  and  $u_{*,a}$  are the surface-layer wind and friction velocity, respectively, at  $\zeta_a = 10 \text{ m}$ ;  $w_* = (\beta Q_* z_i)^{1/3}$  is the convective velocity scale;  $L = -u_{*,a}^3 / \beta \kappa Q_*$  is the Monin–Obukhov stability length with the von Kármán constant  $\kappa = 0.4$ ;  $z_i$  is the boundary layer height;  $z_i/L$  is a bulk stability measure; and  $z_o$  is the roughness matching parameter defined below (31). The run labeled 25<sup>(b)</sup> is carried out with  $U_g = 25 \text{ m s}^{-1}$  but with stationary waves (i.e., bumps), with  $U_a$  and  $u_{*,a}$  computed at  $\zeta = 30 \text{ m}$ . Surface heat flux  $Q_* = 0.01 \text{ K m s}^{-1}$  and buoyancy parameter  $\beta = g/\theta_o = 3.38 \times 10^{-2} \text{ m s}^{-2} \text{ K}^{-1}$  in all simulations.

$U_g$ (m s <sup>-1</sup> )	$C_p/U_a$	$U_a$ (m s <sup>-1</sup> )	$u_{*,a}$ (m s <sup>-1</sup> )	$w_*$ (m s <sup>-1</sup> )	$-L$ (m)	$z_i$ (m)	$-z_i/L$	$z_o \times 10^4$ (m)
5	4.2	4.32	0.148	0.515	24	405	16.9	0.4
10	2.4	7.61	0.298	0.532	196	445	2.28	3.1
20	1.3	13.6	0.545	0.553	1197	501	0.42	4.4
25	1.1	16.1	0.647	0.566	2001	536	0.27	4.7
25 <sup>(b)</sup>	—	17.5	0.683	0.566	2356	535	0.23	10.1

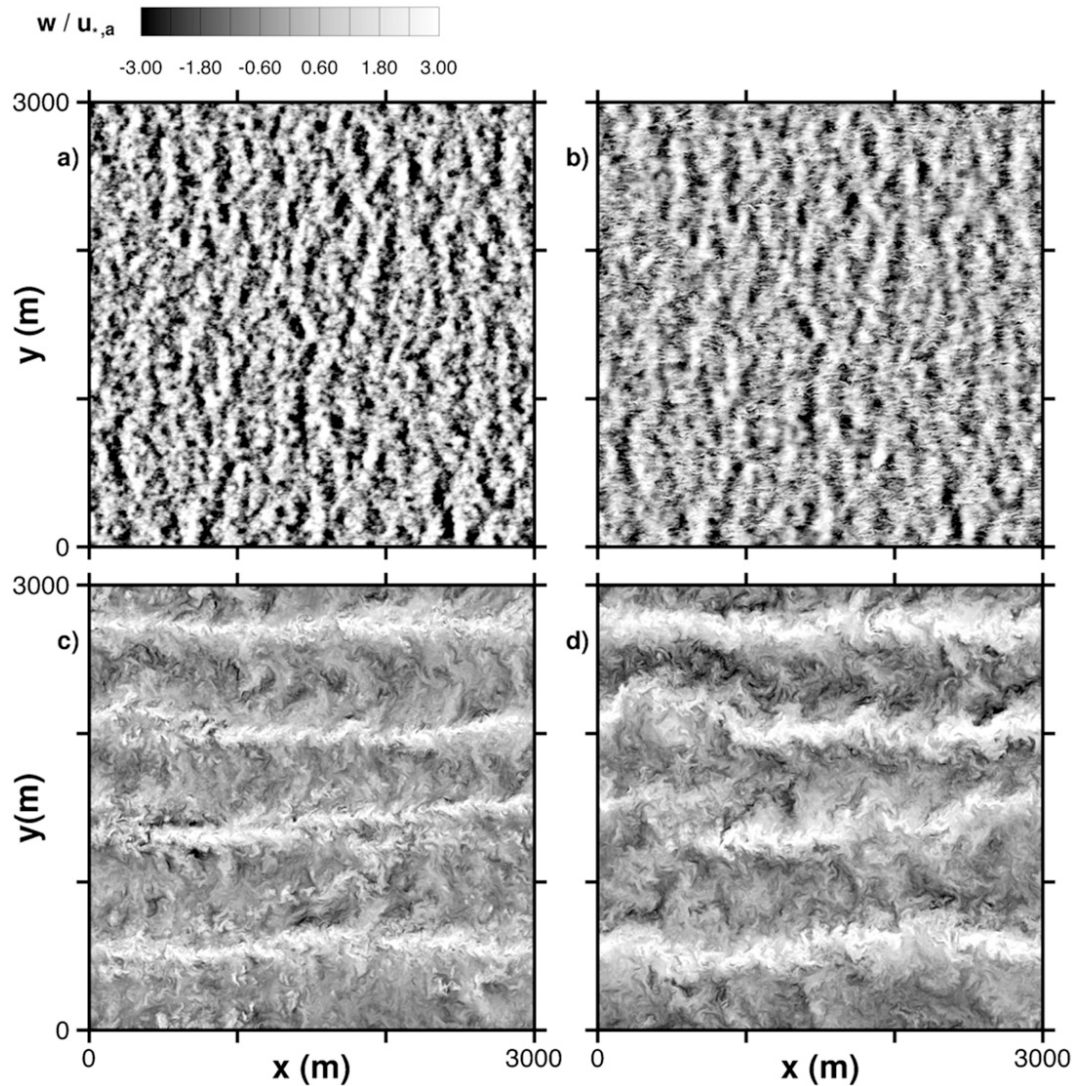


FIG. 4. Instantaneous vertical velocity  $w$  normalized by  $u_{*,a}$  in an  $x$ - $y$  plane at vertical levels  $\zeta =$  (a) 2.5, (b) 9.6, (c) 90.5, and (d) 208.4 m, with wave age  $C_p/U_a = 2.4$  and  $U_g = 10 \text{ m s}^{-1}$ . Notice the smooth transition in the vertical velocity field from wave-impacted turbulence near the wavy boundary to shear-convective streaks in the middle of the MABL.

vary markedly with time as found in the recent High-Resolution Air–Sea Interaction (HiRes) field campaign; see Grare et al. (2013). Over the short 2-week observational period, the HiRes MABL regime featured moderate to high surface-layer winds varying from 5 to  $15 \text{ m s}^{-1}$ , with weak stability conditions just left (unstable) and right (stable) of neutral. The high surface-layer winds generated large waves with significant wave height ( $H_s > 4.5 \text{ m}$ ) over several days. And because of the variability in the wind conditions, wave age varied from growing waves ( $C_p/U_a < 1.2$ ) to swell-dominated conditions ( $C_p/U_a > 4$ ). This wide and complex observational space can only be sparsely explored with finite computational resources. Thus, for our LES study, we

focus on a series of simulations of a weakly unstable MABL, mimicking the forcing and wave conditions in HiRes, with varying geostrophic wind  $U_g = (5, 10, 20, 25) \text{ m s}^{-1}$  and constant surface heating  $Q_* = 0.01 \text{ K m s}^{-1}$ . The addition of a slight amount of surface heating serves two purposes: it helps to initiate the turbulence and thereby skips the long spinup time of a purely neutral simulation, and second, it allows an investigation of the large-scale MABL motions generated by shear and convection in the presence of surface waves. For the wave spectrum, we choose wind-wave equilibrium conditions  $C_p/U_a = 1.2$  and  $U_a = 15 \text{ m s}^{-1}$  with the resulting significant wave height  $H_s = 6.4 \text{ m}$ . This suite of simulations, although idealized, allows us to carry out a process study with wave age

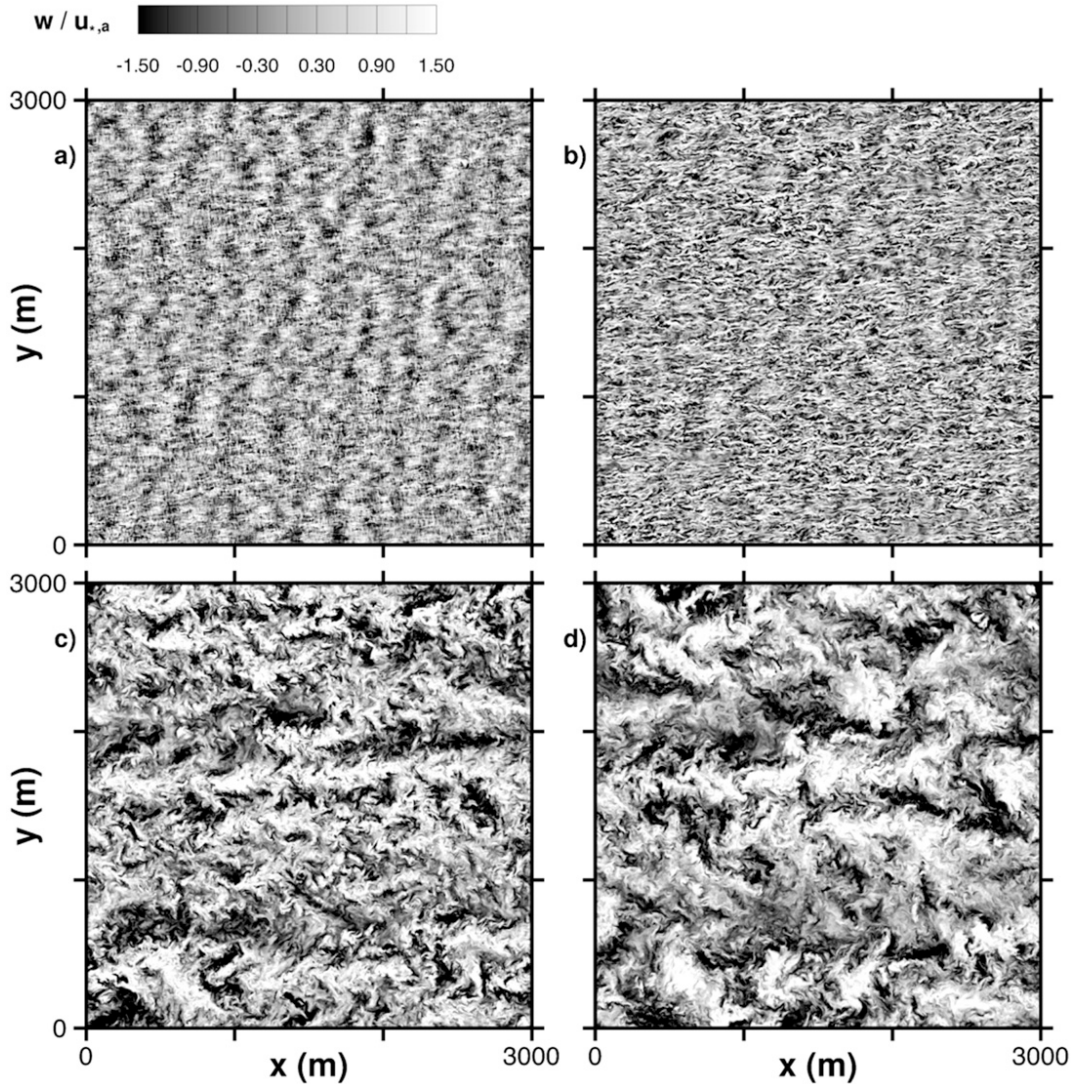


FIG. 5. Instantaneous  $w/u_{*,a}$  at the same vertical levels as in Fig. 4 for  $C_p/U_a = 1.1$  and  $U_g = 25 \text{ m s}^{-1}$ . The color bar range for  $w/u_{*,a}$  is narrower compared to that used in Fig. 4.

varying from near wind-wave equilibrium to swell dominated in the presence of large surface waves. Here wave-age variations are generated solely by varying  $U_g$ . For our comparisons, we also generate a solution for stationary waves (i.e., fixed bumps), with  $U_g = 25 \text{ m s}^{-1}$ .

A typical snapshot of the wave field generated by (13) and used in the LES is shown in Fig. 2. Broadly, the image reveals a preference toward long crested waves; that is, waves with aspect ratio long in the direction perpendicular to the winds; a consequence of the directional wave spectrum. A closer examination of the wave field shows rich multiscale variations in both  $x$  and  $y$  directions. Horizontal 1D spectra of the wave height variance in the  $x$  and  $y$  directions, given in Fig. 3, confirm the horizontal anisotropy of the wave field at low wavenumber.

The spectra exhibit a power law of  $k^{-5/2}$  at small scales (high wavenumbers).

To capture the widest possible range of scales in a full MABL we utilize a computational box of size  $(L_x, L_y, L_z) = (3000, 3000, 800) \text{ m}$  and discretize the domain using  $(N_x, N_y, N_z) = (1024, 1024, 512)$  grid points (i.e.,  $0.5 \times 10^9$  grid points). The horizontal grid spacing  $\Delta\xi = \Delta\eta = 2.93 \text{ m}$  and the first vertical level is nominally located 1 m above the water surface. A nonuniform vertical grid distribution is generated by smooth algebraic stretching with the spacing ratio between any two adjacent cells  $\Delta\zeta_{i+1}/\Delta\zeta_i \approx 1.009$ . A typical vertical  $x$ - $z$  slice of the time-varying surface-fitted grid mesh near the water surface is given in Fig. 2. The image clearly shows how the mesh translates vertically in response to the



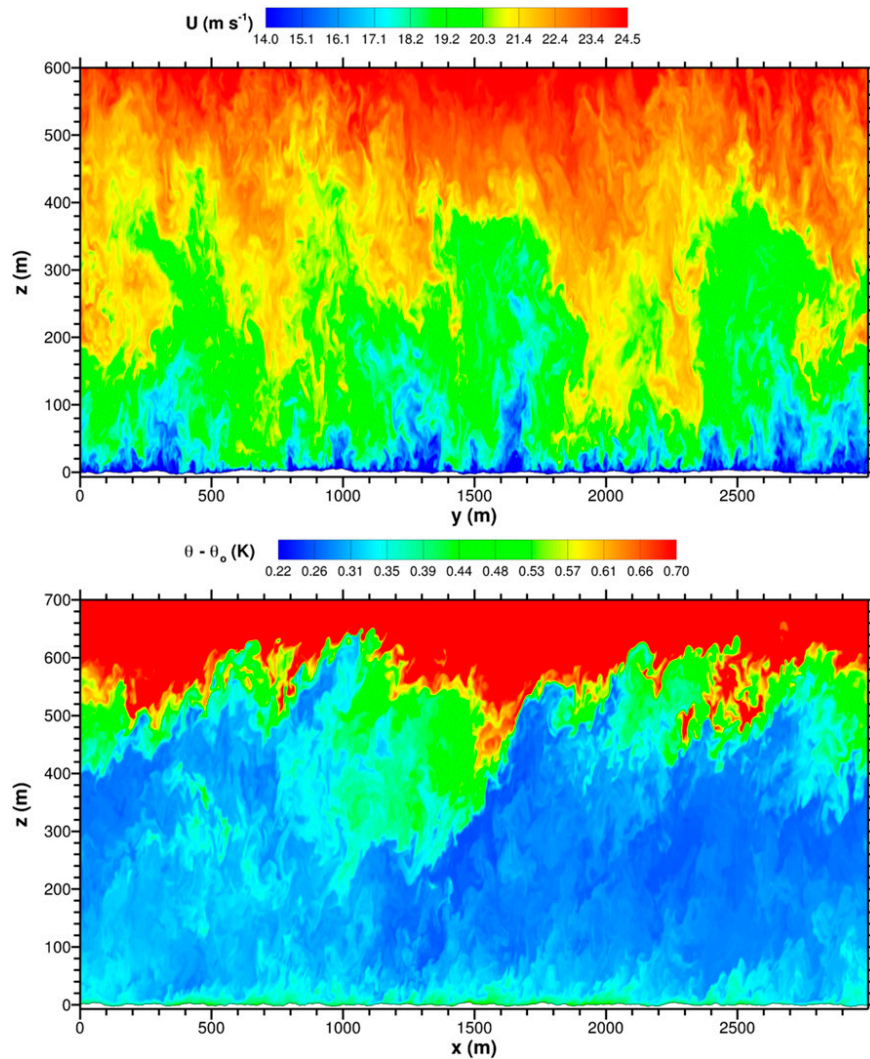


FIG. 6. (top) The instantaneous streamwise velocity contours in a  $y$ - $z$  plane. Notice the large-scale shear-convective rolls and the eruption of low-speed fluid near the lower wavy boundary. (bottom) Potential temperature contours in an  $x$ - $z$  plane where the winds are mainly from left to right. Notice the large-scale engulfment (entrainment) event near  $x \sim 1200$  m and the small-scale detrainment events near  $(x, z) \sim (2500, 550)$  m. Simulation is for  $U_g = 25 \text{ m s}^{-1}$  and  $Q_* = 0.01 \text{ K m s}^{-1}$ .

wide range of wave modes at the lower boundary. We find that over most of the domain the mesh skewness is low as the wave slopes ( $h_x, h_y$ ) are typically smaller than 0.35. The initial temperature sounding is constant,  $\theta = 290 \text{ K}$  up to an inversion height  $z_i = 300 \text{ m}$ ; beyond this initial inversion height,  $\theta$  increases linearly at  $3 \times 10^{-3} \text{ K m}^{-1}$ , and the Coriolis parameter  $f = 10^{-4} \text{ s}^{-1}$ . The unresolved surface waves are simply modeled by a fixed surface roughness  $z_o = 0.0002 \text{ m}$ , noting that the dynamic modeling approach can be used to reduce the sensitivity to the grid resolution (Yang et al. 2013). Random perturbations in velocity and potential temperature are introduced to trigger turbulence. Statistics

are obtained by a combination of space and time averages. Because of horizontal periodicity, spatial averages are computed by area averaging over  $\xi$ - $\eta$  surfaces (i.e., along a surface of constant  $\zeta$ ). Averaging in a wave-following coordinate system allows us to compute statistics down to the water surface (i.e., between and below the wave crests). The resulting vertical profiles are further averaged in time; these averages are indicated by angle brackets. We emphasize that there is no net flow across the wavy lower boundary [i.e.,  $W(x, y, \zeta = 0) = 0$ ], and, hence, no net accumulation of mass in the computational domain similar to flat wall boundary layers. Our time averaging is taken over a time period when the



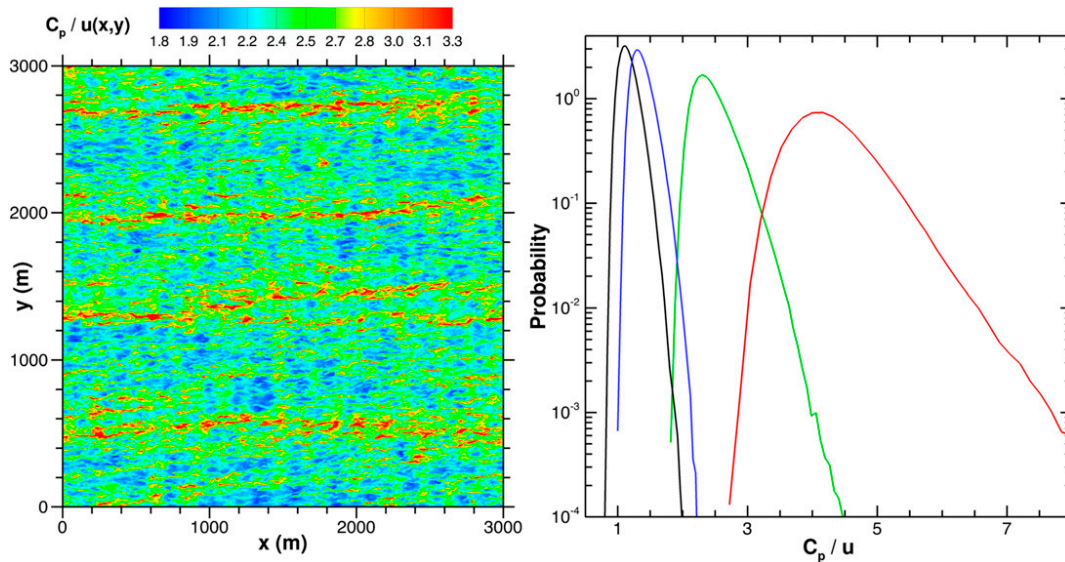


FIG. 7. (left) The variation of local wave age  $C_p/u(x, y)$  across the horizontal domain at height  $\zeta_a = 10$  m. The simulation is for  $U_g = 10 \text{ m s}^{-1}$  and  $Q_* = 0.01 \text{ K m s}^{-1}$  with average bulk wave age  $C_p/U_a = 2.4$ . Large (small) wave age indicated by red (blue) contours occurs beneath the updrafts (downdrafts) and is induced by the large-scale shear-convective rolls. (right) The probability density function of  $C_p/u$  for simulations with average wave age  $C_p/U_a = 1.1$  (black), 1.3 (blue), 2.4 (green), and 4.2 (red).

boundary layer is quasi stationary and grows slowly only because of entrainment at the boundary layer inversion. The top of the MABL  $z_i$  is marked by a steep stable gradient in potential temperature and is estimated using the maximum-gradient method described in Sullivan et al. (1998). Table 1 lists bulk properties of the simulations.

Because of the very high computational expense, these LESs are first started with a flat lower boundary layer (no waves) and run until the turbulence is in near statistical equilibrium. Then the propagating surface waves are “linearly grown” to their full height over a period of about 400 s. This strategy significantly reduces the computational cost and also minimizes non-physical transients in the solutions that can arise by suddenly introducing the surface waves. The simulations with waves are run for more than 100 000 time steps using restart volumes with fully developed turbulence. The iteration count in the pressure Poisson solver is set to 30. Each run consumes more than  $10^6$  h running on 2048 computational cores.

#### b. Flow visualization

To gain an overall impression of the flow patterns in the MABL, a small subset of images generated from our simulations is provided in Figs. 4–7. We find vertical velocity  $w$  is an excellent diagnostic for visualizing the wide range of scales and wave–MABL couplings captured in our LES. For example, Figs. 4 and 5 illustrate

how the vertical velocity field smoothly transitions from a small-scale wave-impacted regime near the water surface into a large-scale streaky structure in the bulk of the MABL. Inspection of the images shows that, at  $\zeta = 2.5$  m,  $w$  tends to closely mimic the long-crested north–south orientation of the streamwise-propagating wave field seen in Fig. 2, this holds for all wave ages. At  $\zeta = 9.6$  m, the wave-induced pattern in  $w$  is visible but gradually blurs with decreasing wave age (i.e., as the background turbulence grows in intensity and the winds and waves approach equilibrium).

At high levels in the MABL,  $\zeta > 90$  m, the dominant flow pattern in  $w$  in each simulation switches from the near-surface north–south orientation into a streaky structure mainly aligned in the streamwise (west–east) direction. Animations clearly show the long-lived temporal and large-scale spatial coherence of these structures. Similar shear-convective-generated streaks (or rolls) are present in weakly stratified boundary layers over land in a more unstable range  $-z_i/L \sim 1.5$  (e.g., Moeng and Sullivan 1994; Fedorovich et al. 2004) but are pervasive in our simulations of the MABL even with the generally higher winds and weaker surface heating (i.e.,  $-z_i/L < 0.5$ ). Further evidence for shear-convective rolls in the MABL is provided in the cross-cutting view (a  $y$ – $z$  plane) of Fig. 6 for the simulation very near neutral conditions,  $C_p/U_a = 1.1$  and  $-z_i/L = 0.27$ . The roll organization over the entire MABL is even stronger for simulations with  $-z_i/L = 0.42$  and

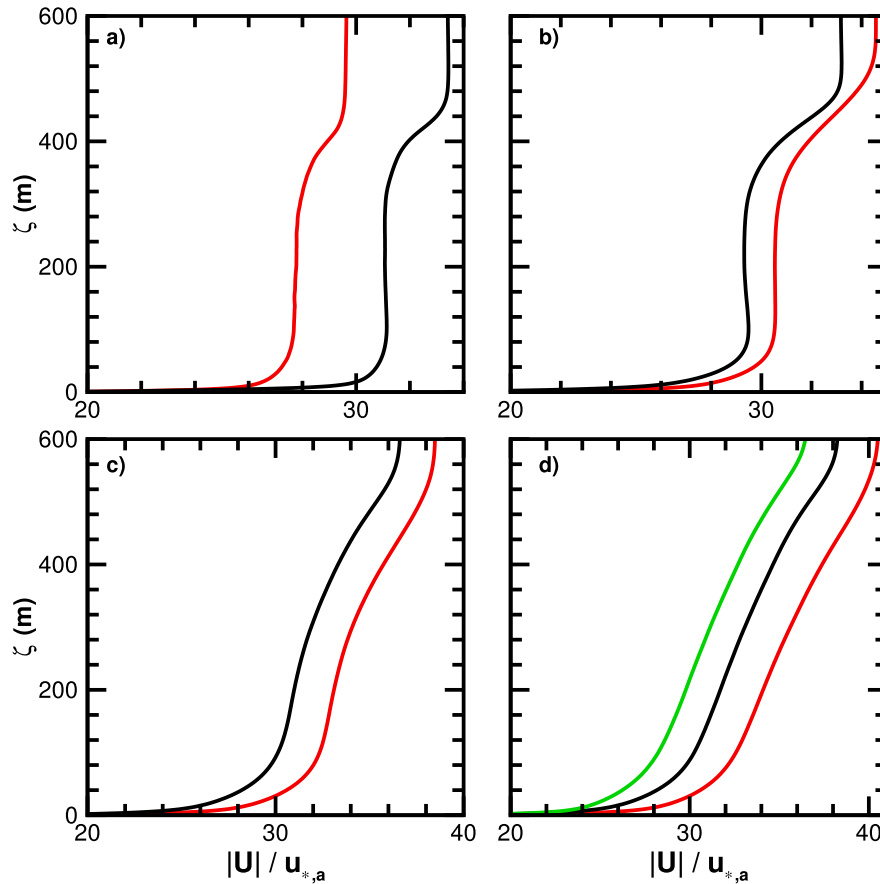


FIG. 8. Vertical profiles of normalized average wind speed for different values of wave age  $C_p/U_a =$  (a) 4.2, (b) 2.4, (c) 1.3, and (d) 1.1. The friction velocity at the reference height  $u_{*,a}$  is used for normalization. The solid red lines are results for a flat surface (no moving waves) while the black lines are results with moving waves. In (d) results for a stationary wavy surface (green line) driven by the same forcing as for the simulations with moving waves are included.

2.28; this can also be inferred from the  $w$  visualizations in Fig. 4. The descending branch of a roll brings high-speed fluid down to the water surface where the descending flow then turns spanwise and converges with a neighboring roll in a layer just above the wavy surface. Finally, eruptions above the wave field lift low-speed fluid vertically completing a circuit. At  $\zeta_a$ , the ratio of the maximum and minimum values of the horizontal wind  $U_a(x, y)$  differs by more than a factor of 2 because of the large-scale circulations. Thus, the lateral heterogeneity induced by the MABL rolls leads to spatial variability in wave age that is larger and more persistent than that due to turbulent wind gusts as shown in Fig. 7. This variability is readily apparent in the  $w$  patterns underneath a descending branch of a roll circulation where  $u(x, y) > \langle u \rangle$ . The probability density function of wave age shown in Fig. 7 widens considerably in the shear-convective regime (i.e., as the bulk atmospheric stability varies from  $-z_i/L = 0.27$  to 16.9). Figure 6 shows the large impact of

wind shear on MABL entrainment at  $-z_i/L = 0.27$ . Large engulfment events of tropospheric air tilted into the streamwise direction extend deep into the middle MABL (see section 4d and Fig. 13). These engulfment events are frequently observed to be accompanied by intermittent detrainment of MABL air.

### c. Winds

One of the outstanding questions in MABL dynamics is the interaction between surface waves and the overlying winds, and the vertical extent of the region impacted by surface waves, the so-called wave boundary layer (Sullivan et al. 2008; Sullivan and McWilliams 2010). A separate but related topic is the adequacy of rough-wall Monin–Obukhov (MO) similarity theory, typically applied to homogeneous land surfaces, to predict surface fluxes based on winds measured at a standard reference height. To investigate these questions, we follow a large body of observational studies

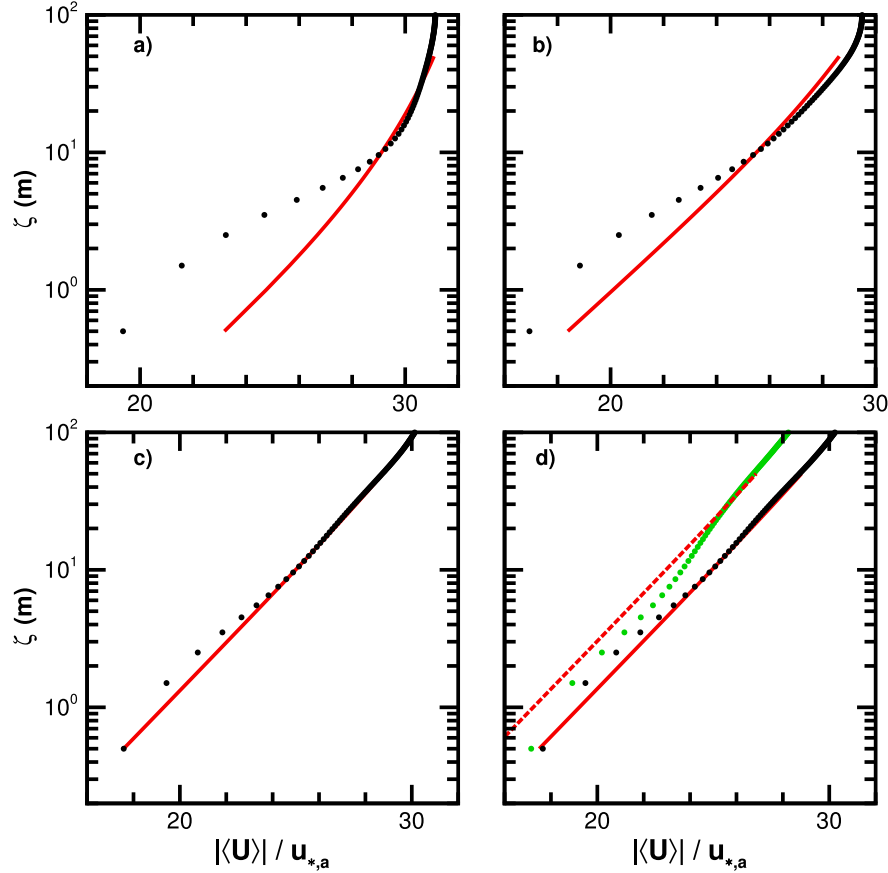


FIG. 9. Comparison of the vertical profiles of normalized wind speed from LES (solid bullets) and predictions from Monin–Obukhov similarity theory shown by the solid red curves.  $C_p/U_a =$  (a) 4.2, (b) 2.4, (c) 1.3, and (d) 1.1. LES and MO theory are matched at  $\zeta_a = 10$  m. In (d) results for a stationary wavy surface (green bullets) and an MO fit (dashed red line) where the matching height is  $\zeta = 30$  m are included.

(e.g., Fairall et al. 2003) and use the LES atmospheric conditions at the reference height  $\zeta_a = 10$  m to define a nondimensionalizing friction velocity  $u_{*,a}$ . First, we compute vertical momentum fluxes  $\mathbf{u}_{f,a}$  based on time and space averaging in (8c) and (9a) at  $\zeta_a$ :

$$u_{f,a} = -\left\langle u(W - z_t) + \frac{p^*}{J} \frac{\partial \zeta}{\partial x} + \frac{\tau_{1k}}{J} \frac{\partial \zeta}{\partial x_k} \right\rangle_a, \quad (29a)$$

$$v_{f,a} = -\left\langle v(W - z_t) + \frac{p^*}{J} \frac{\partial \zeta}{\partial y} + \frac{\tau_{2k}}{J} \frac{\partial \zeta}{\partial y_k} \right\rangle_a. \quad (29b)$$

These momentum fluxes include contributions, from left to right, by resolved turbulence  $t_f$ , pressure  $p_f$ , and subgrid-scale turbulence  $s_f$  terms; (29) includes small but important pressure–wave slope correlations  $p_f$  to account for the vertical variation of the horizontal gridlines  $\xi$  and  $\eta$  in physical space. The average fluxes in (29) are next aligned with the average winds  $\langle \mathbf{u}_a \rangle$  and thus

$$u_{*,a} = \left( \frac{-\mathbf{u}_{f,a} \cdot \langle \mathbf{u}_a \rangle}{|\langle \mathbf{u}_a \rangle|} \right)^{1/2} \quad (30)$$

serves as our LES estimate of the friction velocity (or wind stress  $u_{*,a}^2$ ) at  $\zeta_a$ . Note that, in arriving at (30), there is no assumption of a constant-flux layer.

Figures 8 and 9 compare vertical profiles of the nondimensional mean wind speed  $|\langle \mathbf{u} \rangle|/u_{*,a}$  over the bulk of the boundary layer and also near the water surface for varying wave age. In Fig. 9 we also include a wind profile predicted from (MO) similarity theory (Wyngaard 2010):

$$U_{\text{MO}}(\zeta) = \frac{u_{*,a}}{\kappa} \left[ \ln \left( 1 + \frac{\zeta}{z_o} \right) + \psi(\zeta/L) \right], \quad (31)$$

where the stability function  $\psi(\zeta/L)$ , given by Large et al. (1994), accounts for the slight surface heating. The vertical coordinate is distance from the water surface  $\zeta$ ,

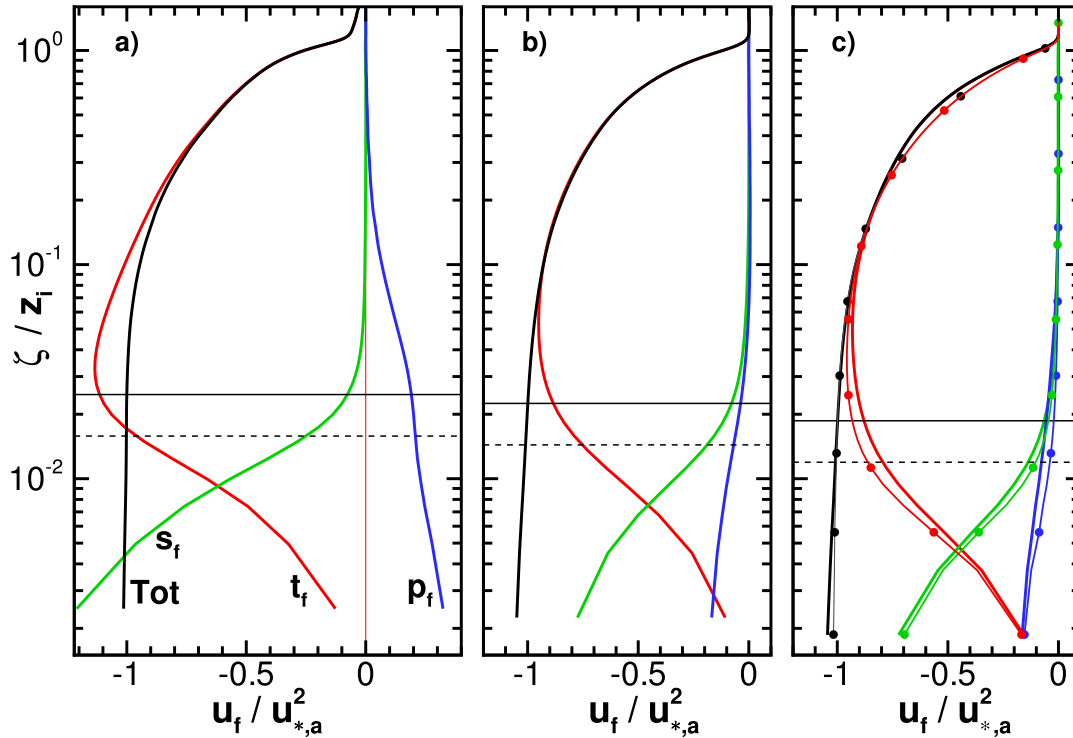


FIG. 10. Vertical profiles of the normalized flux terms contributing to streamwise ( $u_f$ ) momentum over the entire marine boundary layer for varying wave age. Wave age = (a) 4.2, (b) 2.4, and (c) 1.1. The colors in each panel are resolved turbulent ( $t_f$ ; red), pressure–wave slope ( $p_f$ ; blue), and subgrid-scale ( $s_f$ ; green) fluxes, and their sum the total (Tot) flux (black). The nondimensional heights  $\zeta_a/z_i$  and  $H_s/z_i$  are shown by thin solid and dashed horizontal lines, respectively. The total flux is approximately constant in the marine surface layer but individual flux components vary markedly with wave age. Notice the presence of wave-driven winds (positive form stress) in the high-wave-age simulation in (a). In (c), results for the simulation with stationary waves (bumps) are included with results indicated by thin lines marked with solid bullets. In this simulation, the normalizing wind stress is evaluated at  $\zeta = 30$  m or  $\zeta/z_i = 0.0561$ .

not from the mean water level. To compare MO theory with LES, we use  $u_{*,a}$  defined by (30) and treat  $z_o$  in (31) as a matching parameter [i.e., we pick  $z_o$  so that, at the reference height,  $U_{MO}(\zeta_a) = |\langle \mathbf{u}_a(\zeta_a) \rangle|$ ].

Inspection of the bulk wind profiles in Fig. 8 reveals a clear dependence on wave age. In the simulation with wave age  $C_p/U_a = 4.2$ , the winds in the bulk of the boundary layer are faster than for a similar flow above a flat (stationary) boundary. In this nonequilibrium wind-wave regime, the surface-layer winds are accelerated (pushed forward) by fast-moving waves, thereby creating a wave-driven wind. For the wave spectrum in Fig. 3, a large fraction of the wave modes are traveling in the same direction as, but faster than, the local surface-layer winds, roughly all wave modes with  $\lambda > 16$  m propagate with speed  $c > 5$  m s $^{-1}$ , or  $c/u_{*,a} > 34$ . The mechanics of the wave-driven wind process are analyzed in a much idealized LES by Sullivan et al. (2008) and Nilsson et al. (2012) where swell is simply modeled as a single monochromatic surface wave.

Broadly, we find dynamical similarities in the current LES with a much more realistic full wave spectrum. The key dynamics leading to wave-driven winds is the pressure form stress that acts as a thrust (as opposed to a drag) on the overlying winds at large wave age (see Fig. 10). The overall well-mixed shape of the wind profiles observed in Fig. 8a is a consequence of the relatively light winds forced by a small amount of surface heating; the stability measure  $-z_i/L = 16.9$  indicates that convection is significant. In our simulations, wave age is varied from 4.2 to 1.1 by increasing  $U_g$  from 5 to 25 m s $^{-1}$ . On the approach to wind-wave equilibrium, the bulk boundary layer winds slow down compared to their counterparts over a flat lower boundary; a consequence of a reversal in the pressure form stress switching sign from positive to negative. With increasing geostrophic winds and surface heating held constant, the wind profiles gradually assume a shape typical of shear-dominated boundary layers (e.g., Moeng and Sullivan 1994) but with higher drag compared to a flat



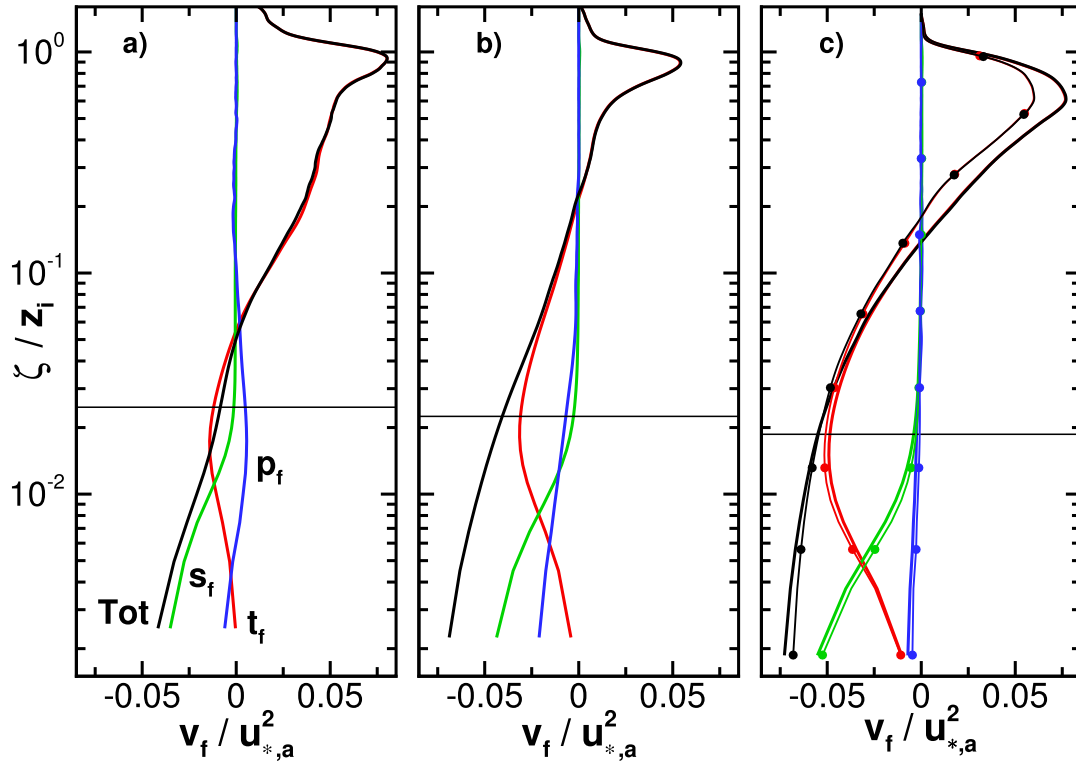


FIG. 11. Vertical profiles of the flux terms contributing to spanwise ( $v_f$ ) momentum. The conditions and labeling are as in Fig. 10, but with a narrower range of values along the abscissa.

stationary wall,  $u_{*,a}$  and  $z_o$  both increase with  $U_g$  as shown in Table 1.

A comparison between the LES wind profiles and the MO fit in (31) in the near-surface region further illustrates wave effects (see Fig. 9). As expected, the largest discrepancy between LES and MO wind profiles occurs in the situation with nonequilibrium winds and waves (i.e., light winds above fast-moving waves). The MO fit predicts noticeably faster surface-layer winds below  $\zeta_a$  compared to LES. This discrepancy cannot be simply reconciled by adjustment of the matching height [e.g., choosing  $\zeta_a = 5$  m overpredicts (underpredicts) the wind speed below (above)  $\zeta_a$ ]. Observations reported by Höglström et al. (2013) also suggest that the wind profile near the water surface deviates markedly from MO predictions in swell-dominated regimes. The deficiency of MO similarity theory is a consequence of missing dynamics (i.e., upward vertical momentum flux from large surface waves to the atmosphere). Hanley and Belcher (2008) propose a 1D column model that captures some of the effects of wave-driven winds. The agreement between the LES winds and MO fit are remarkably close below  $\zeta_a$  and also in a limited zone above  $\zeta_a$  as the winds and waves approach equilibrium. In this regime, the peak of the spectrum is traveling about 20%

faster than the surface winds and then, very broadly, the remainder of the smaller-scale wave modes acts as a slow-moving momentum sink (or drag). The wind profiles displayed in Figs. 8d and 9d further illustrate that even at wind-wave equilibrium conditions flow over moving waves differs from its counterpart over an identical but stationary wave spectrum. In the situation of stationary bumps, the wavy surface is rougher with larger values of  $u_{*,a}$  and  $z_o$  and the vertical height where the wind profile blends into a log-linear profile is higher, near  $\zeta = 30$  m. In flow over stationary bumps, the winds effectively feel all wave modes as roughness elements. The robustness of the MO fit in (31) clearly needs further evaluation over a broader range of forcings, including more common nonequilibrium wind-wave states (Hanley et al. 2010) using representative wave spectra as discussed here. For example, LES with weak winds opposing waves are markedly different than simulations with wave-driven winds (results not shown).

#### d. Momentum and scalar fluxes and velocity variances

Implicit in the application of MO theory to flow over ocean waves is the assumption that  $\zeta_a$  is located above any wave-induced layer but remains sufficiently close to

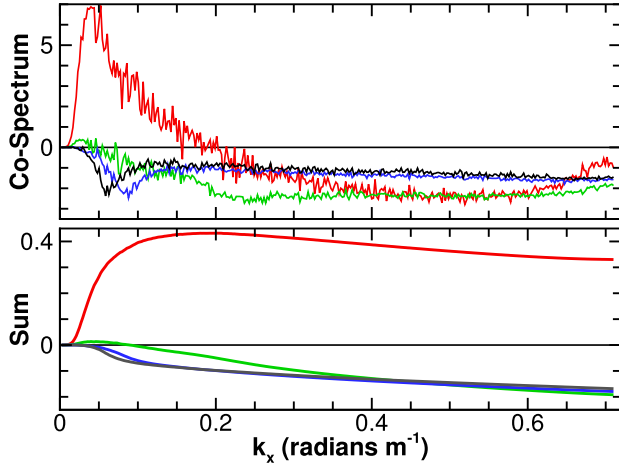


FIG. 12. (top) The cospectrum between pressure  $p^*$  and wave slope  $\zeta_x/J$  at the water surface normalized by  $k_x 10^4 / u_{*a}^2$ . (bottom) The running sum of the cospectrum over  $k_x$  wavenumbers normalized by  $u_{*a}^2$ . At the highest wavenumber, the running sum is equal to the normalized flux  $p_f / u_{*a}^2$  given in Fig. 10. The colored lines correspond to  $C_p / U_a = 4.2$  (red), 2.4 (green), 1.3 (blue), and 1.1 (black). The wavenumber  $k_x \sim 0.03$  (rad  $m^{-1}$ ) corresponds to the peak in the wave height spectrum shown in Fig. 3.

the water surface so that the change in the average vertical momentum fluxes with height is negligible (i.e., there is a constant-flux layer). In the convective atmospheric boundary layer over land, above the constant-flux layer and below the entrainment zone, the momentum and scalar fluxes decrease almost linearly from their surface values [see p. 215 in Wyngaard (2010)]. The constant-flux-layer assumption is the cornerstone that allows field studies to infer the stress at the water surface using observations at  $\zeta_a$ , and it is also a widely adopted assumption by second-order closure models (e.g., Gent and Taylor 1976; Makin et al. 1995) and in turbulence simulations (e.g., Sullivan et al. 2000; Yang et al. 2013; Suzuki et al. 2013). Here we use LES results to test the validity of the constant-flux layer assumption for the wavy MABL.

Contributions to the  $u$  and  $v$  momentum equations from the fluxes  $t_f$ ,  $p_f$ , and  $s_f$ , essentially the time- and space-averaged right-hand-side terms of (29a) and (29b), are summed and compared in Figs. 10 and 11 for varying wave age over the full depth of the MABL. Remarkably, we find the total flux, computed in wave-following coordinates, for the dominant  $u$  component is indeed nearly constant over the interval  $0 < \zeta < \zeta_a$  in our simulations. The result appears robust despite the large value of significant wave height,  $H_s / \zeta_a \sim 0.64$ . Examination of the results over the interval  $0 < \zeta < \zeta_a$  shows that the total stress at the surface is slightly larger (more negative) than at  $\zeta_a$ . A small vertical flux

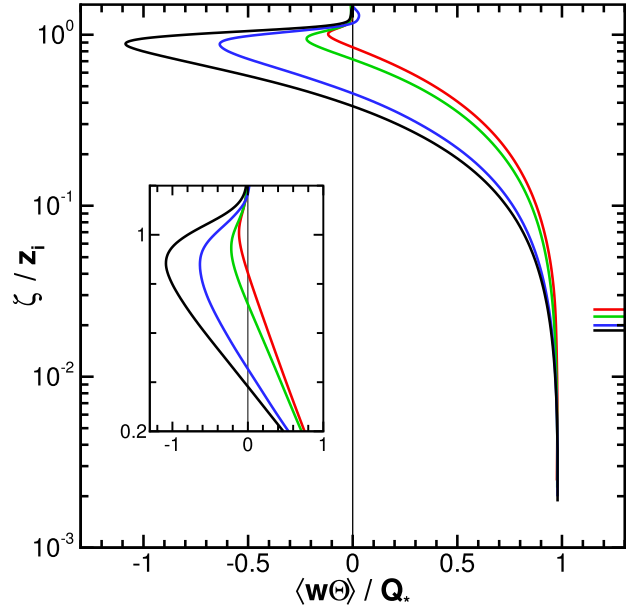


FIG. 13. Vertical profiles of total (resolved plus SGS) vertical buoyancy flux normalized by the surface value  $Q_*$  for varying geostrophic wind. The colored lines correspond to wave ages of 1.1 (black), 1.3 (blue), 2.4 (green), and 4.2 (red). The thin colored horizontal lines correspond to the height  $\zeta_a / z_i$ . The main plot emphasizes the constant-flux layer near the wavy boundary. The inset shows the linear variation of the buoyancy flux with height over the bulk of the MABL and the large increase in normalized entrainment with increasing wind speed.

divergence for both  $u$  and  $v$  components, about 8% of  $u_{*a}^2$ , is required to balance the Coriolis forces and the large-scale pressure gradients that appear in (8c). A noticeable decrease with height in the  $u$  momentum fluxes starts at about  $\zeta / z_i \approx 0.1$ . The near-constant-flux layer observed in Fig. 10 is not imposed but is a consequence of the fine mesh and resolved dynamics in the LES. Since the present SGS model is an adaption of a standard TKE model (Moeng and Wyngaard 1988), we expect other comparable SGS models will generate similar solutions on a fine mesh.

Figures 10 and 11 also illustrate important wave effects. The partitioning of the total momentum flux between  $t_f$ ,  $p_f$ , and  $s_f$  is strongly height and wave-age dependent. For example, in the simulation with  $C_p / U_a = 4.2$ , wave effects are readily apparent in the turbulent and pressure flux contributions well above  $\zeta_a$  extending as high as 100 m or more (also see Figs. 17 and 18); on average, they tend to counterbalance each other for  $\zeta > \zeta_a$ . The shifting flux balance between  $t_f$ ,  $p_f$ , and  $s_f$  below  $\zeta_a$  is a consequence of the scale content of the wave spectrum and the magnitude of the surface winds. For the simulation with  $C_p / U_a = 4.2$ , the longest wavelength modes in the wave spectrum propagate

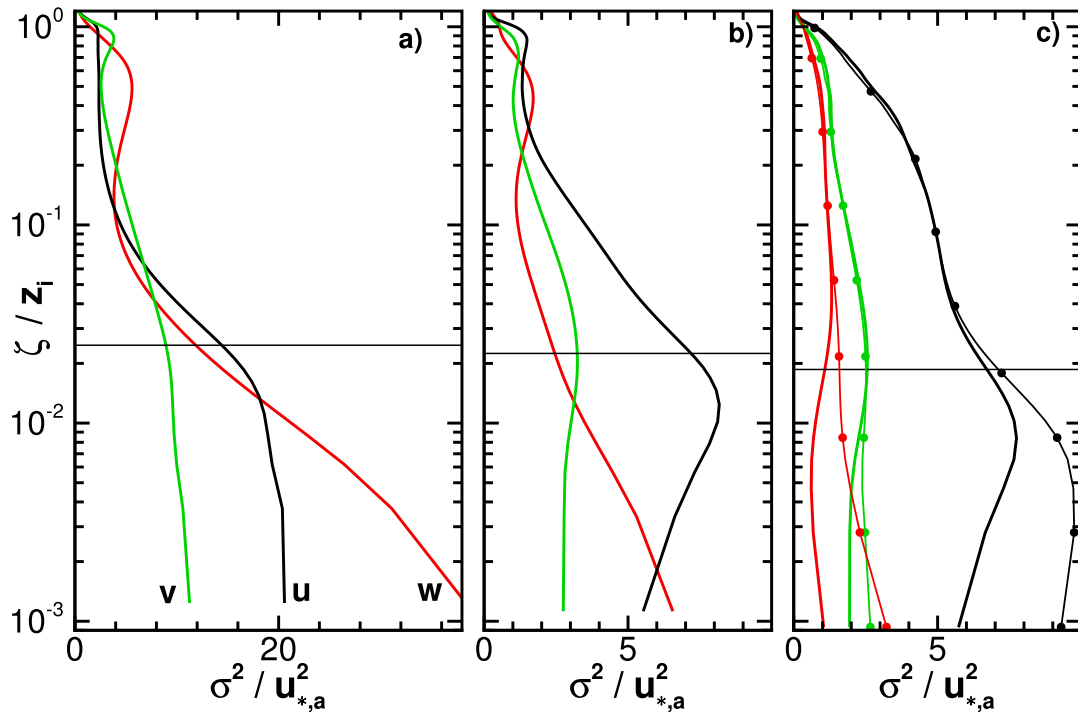


FIG. 14. Vertical profiles of resolved variances ( $\sigma_u^2$ ,  $\sigma_v^2$ ,  $\sigma_w^2$ ) normalized by the wind stress at the 10-m reference height over the entire MABL. Wave age is (a) 4.2, (b) 2.4, and (c) 1.1. The thin horizontal line is the reference height  $\zeta_a/z_i$ . In (c) results for the simulation with stationary waves are indicated by thin lines marked with solid bullets. Note that the abscissa range changes between (a) and (b).

rapidly compared to the surface winds and at  $\zeta = 0$  generate net upward momentum flux through a positive pressure–wave slope correlation. This positive form stress is counterbalanced by a large negative SGS contribution resulting in a surface stress that is nearly equal to its value at  $\zeta_a$ . Note that the resolved turbulent flux equals zero at  $\zeta = 0$  because of no flow through the water surface. The implication for this large wave-age simulation is that small-scale waves, smaller than are resolved by the LES mesh, slow the winds at  $\zeta = 0$ . As we decrease the wave age, by increasing the geostrophic winds, the momentum flux partitioning smoothly shifts between  $t_f$ ,  $p_f$ , and  $s_f$ . The large-scale waves support small form stress as they are propagating at a speed close to the surface winds, and then the intermediate- and smaller-scale wave modes play an important role in supporting the wind stress through a negative pressure–wave slope correlation (form drag). The overall level of the resolved form stress compared to the total wind stress in the LES hints that the high-wavenumber tail of the wave spectrum plays an important role in generating drag at wind-wave equilibrium conditions. The spectral content of the form stress is given by the cospectrum between surface pressure  $p^*$  and wave slope  $\zeta_x/J$  shown in Fig. 12. There is significant wave-age variability with

a local peak and sign changes at low wavenumbers,  $k_x < 0.4 \text{ m}^{-1}$ . Höglström et al. (2009) also suggests that a decomposition of the total drag will include both positive and negative contributions because of swell. However, at high wavenumbers, the small scales, say  $\lambda < 15 \text{ m}$ , add a negative contribution to the overall form stress out to the largest resolved wavenumber in the LES for all wave ages considered (see the bottom panel of Fig. 12). Makin et al. (1995, see their Fig. 4), using a wave growth model, estimate that scales between 0.1 to 10 m carry a large fraction of the form drag.

Figure 13 shows the profile of the total heat flux over the complete MABL. Key points to notice are the dramatic increase in entrainment flux at the MABL top with increasing wind speeds, which is a direct consequence of the large entrainment events observed in the flow visualization of Fig. 6. The (negative) normalized entrainment flux increases from 0.12 to 1.09 as the geostrophic winds increase from 5 to  $25 \text{ m s}^{-1}$ , with the height of the minimum entrainment flux descending with increasing wind speed; the width of the entrainment zone, loosely defined as region where the scalar flux is negative, also expands. The enhancement of entrainment flux at near-neutral conditions is significant and we find similar and larger increases in entrainment flux in

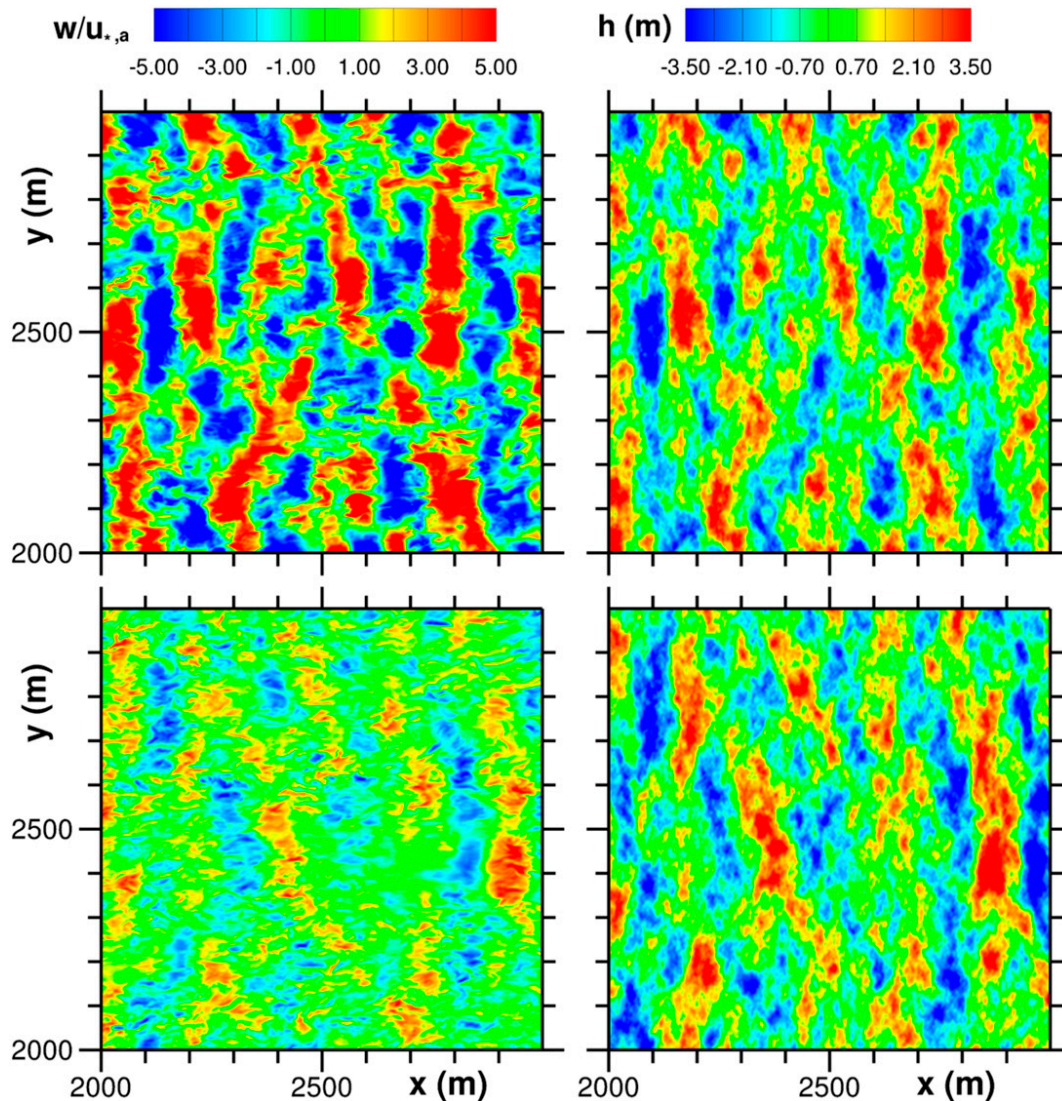


FIG. 15. (left) Snapshots of vertical velocity at a nominal height  $\zeta = 9.57$  m. (right) The companion wave height field.  $C_p/U_a =$  (top) 4.2 and (bottom) 2.4. Vertical velocity is made dimensionless by the wind stress at the reference height  $\zeta_a$  (i.e., the contours are  $w/u_{*,a}$ ). For clarity, only a limited area of the computational domain is shown.

ocean boundary layers driven by hurricane winds and waves (Sullivan et al. 2012). Thus, for the high-wind MABLs examined here, scalar transport is likely influenced by entrainment dynamics. Near and below  $\zeta_a$  the total scalar flux is nearly constant for varying wave age, adding support to the assumption of a constant-flux layer above surface waves.

The resolved turbulence variances  $\sigma_{u,v,w}^2$  shown in Fig. 14 further illustrate wind-wave couplings that vary with wave age: variance is defined as  $\sigma_f^2 = \langle [f(\xi, \eta) - \langle f \rangle]^2 \rangle$ . Notice in the simulation with large wave age, so-called “wave pumping” (McWilliams et al. 1999; Sullivan et al. 2008) by the long wavelength modes in the wave spectrum is vigorous and greatly enhances the variances

generating maxima near the water surface. The surface-enhanced variance decays slowly with increasing  $\zeta$  extending upward to  $\zeta/z_i > 0.1$ . We speculate that near-surface wave pumping might lead to an enhancement of the horizontal  $u$ - and  $v$ -variance components through pressure-strain correlations that are opposite to the usual energy redistribution in a flat-wall boundary layer [see p. 105 in Wyngaard (2010)]. At wind-wave equilibrium, the background shear-generated turbulence overpowers the small-scale wave-induced motions and then the shape and magnitude of the variance profiles are qualitatively similar to those obtained over stationary waves. Also the  $w$  variance in the simulation with  $C_p/U_a = 4.2$  reveals a local maximum slightly



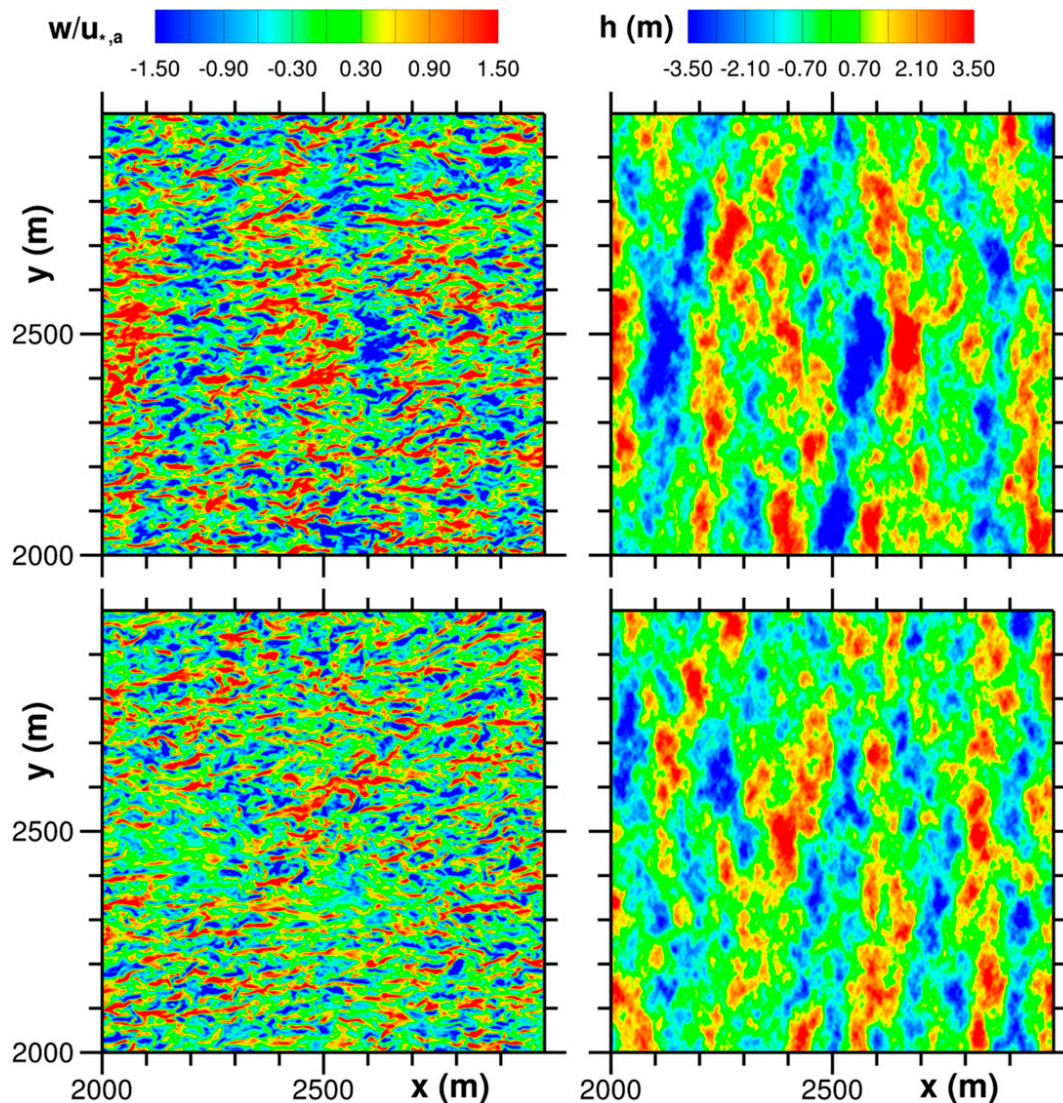


FIG. 16. (left) Snapshots of vertical velocity and (right) wave height.  $C_p/U_a =$  (top) 1.3 and (bottom) 1.1. Labeling and normalization is as in Fig. 15, but with a narrow contour range for the vertical velocity.

below  $\zeta/z_i \sim 0.5$  as expected for a boundary layer forced by convection.

#### e. Wind-wave correlations

Wind-wave studies seek to identify wave-induced (correlated) motions in the turbulent surface-layer winds as this provides insight into wave growth (e.g., Belcher and Hunt 1998; Hristov et al. 1998, 2003; Sajjadi et al. 2014). A qualitative indication of the instantaneous correlation between vertical velocity and the wave field for varying wave age is shown in the snapshots in Figs. 15 and 16; the correlations are quantified in Figs. 17 and 18. The images reflect the atmospheric response for varying wind speeds at a fixed height when the wave spectrum is held constant. At the reference height  $\zeta_a$ , the amplitude

and organization of the wave signal in vertical velocity is clearly wave-age dependent. Despite the randomness of the wind and wave fields, one can readily identify the imprint of the wave field on vertical velocity and notice its decay with decreasing wave age. This is expected based on the flow statistics discussed previously and the visualization presented in section 4b. Close to wind-wave equilibrium ( $C_p/U_a = 1.1$ ), there is only a slight hint of the wave signature in the vertical velocity field. As  $C_p/U_a$  increases past equilibrium, the wave signature gradually emerges and eventually dominates. Past simulations and observations in idealized calculations hint at this dependence and the present calculations with a realistic wave spectrum confirm this wave-age dependence.

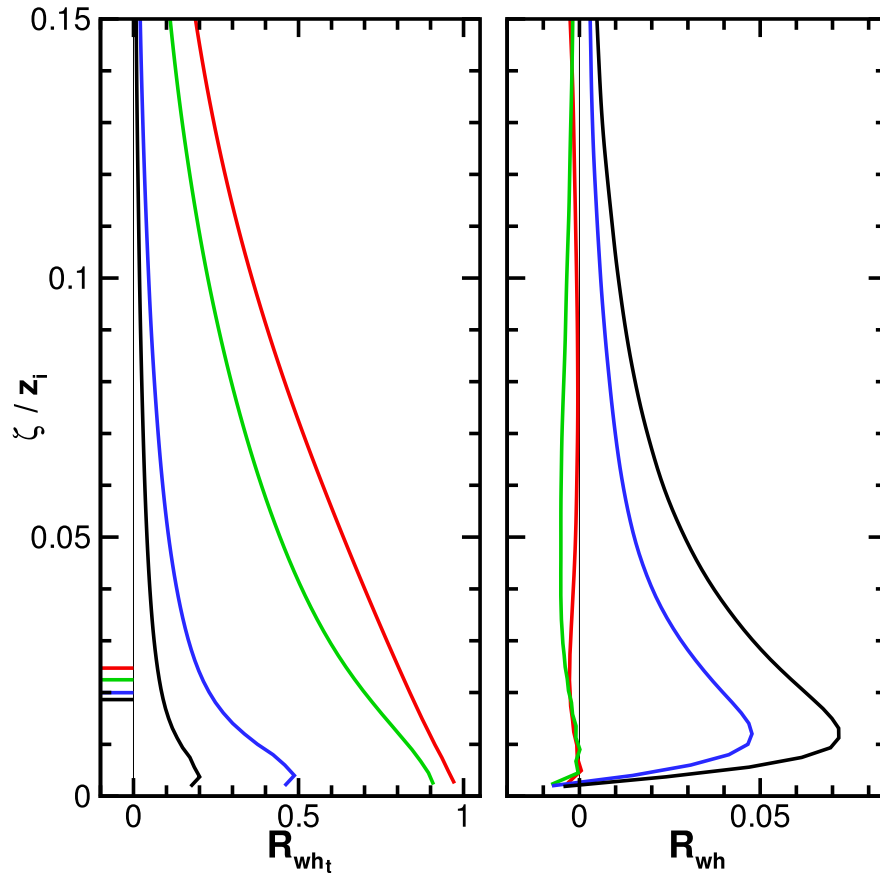


FIG. 17. Vertical profiles of the normalized correlation between resolved vertical velocity and the surface wave field for varying wave age: (left)  $\mathcal{R}_{wh_t}$ , and (right)  $\mathcal{R}_{wh}$ .  $C_p/U_a = 1.1$  (black), 1.3 (blue), 2.4 (green), and 4.2 (red). (left) The thin colored horizontal lines denote the non-dimensional reference height  $\zeta_a/z_i$  above the water surface for that particular simulation.

Figures 17 and 18 show vertical profiles of the wind-wave correlations in our computations. The correlation coefficients are defined as

$$\begin{aligned} \mathcal{R}_{uh} &= \frac{\langle uh \rangle}{\sigma_u \sigma_h}, & \mathcal{R}_{wh} &= \frac{\langle wh \rangle}{\sigma_w \sigma_h}; \\ \mathcal{R}_{uh_t} &= \frac{\langle u \partial h / \partial t \rangle}{\sigma_u \sigma_{h_t}}, & \mathcal{R}_{wh_t} &= \frac{\langle w \partial h / \partial t \rangle}{\sigma_w \sigma_{h_t}}, \end{aligned} \quad (32)$$

where  $\sigma_f$  denotes the standard deviation of variable  $f$ . The correlations illustrate intriguing wave-age dependencies. In large wave-age (nonequilibrium) conditions, the large wave modes propagate quickly compared to the surface winds and their imprint on the atmosphere is best observed in the correlation between vertical velocity and the local time variation of the wave height (i.e.,  $\langle w \partial h / \partial t \rangle$ ). In other words, vertical velocity is nearly  $90^\circ$  out of phase with respect to the wave surface. Note that a finite correlation between  $w$  and  $\partial h / \partial t$  extends well above  $\zeta_a$  and is a clear indication of wave pumping on the atmospheric

winds by the large-amplitude, fast-moving wave modes. This strong correlation disappears near wind-wave equilibrium and subsequently vertical velocity becomes more weakly correlated with wave height in a shallow layer well below  $\zeta_a$ . The normalized correlation between  $u$  and  $(h, \partial h / \partial t)$  is opposite to that of the vertical velocity, as expected. The highest correlation occurs in the swell-dominated regime with wave height. The correlation between  $u$  and the time change of wave height is complex and confined to the layer below  $\zeta_a$  and may be due to critical-layer effects as reported by [Hristov et al. \(1998, 2003\)](#) and [Grare et al. \(2013\)](#). Hence, detailed measurements in a wave-following coordinate system very near the water surface are required to extract wave-induced momentum flux from observational data under wind-wave equilibrium conditions.

## 5. Summary and conclusions

A large-eddy simulation (LES) model that adopts a Boussinesq flow model for the marine atmospheric

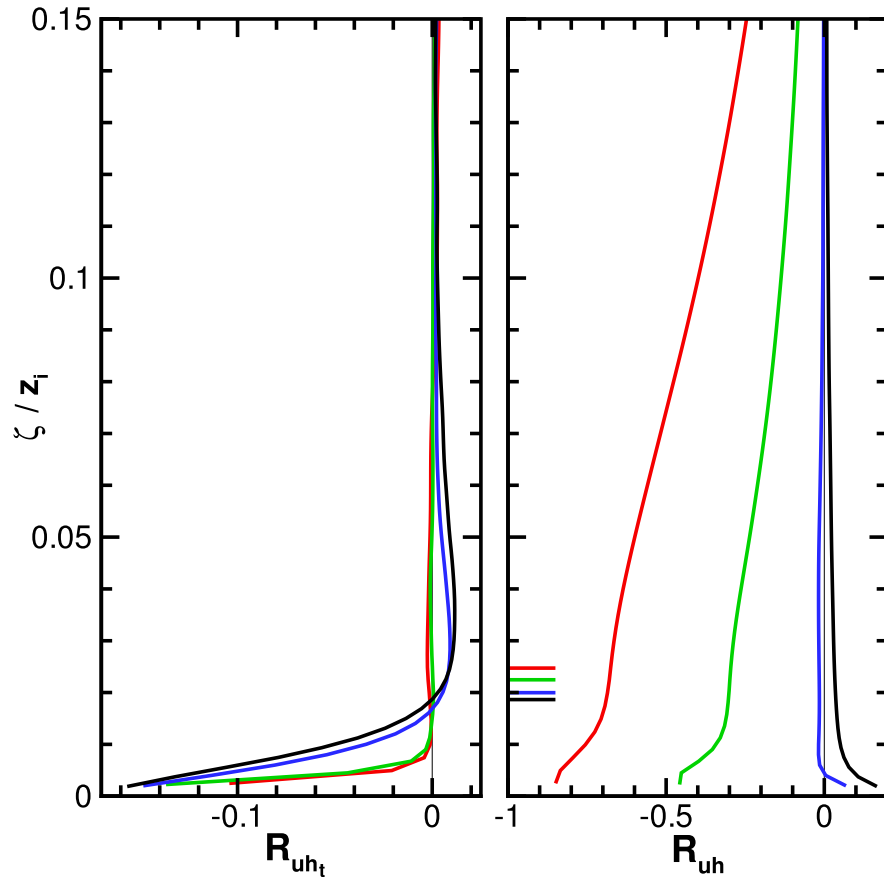


FIG. 18. Vertical profiles of the normalized correlation between resolved streamwise velocity and the surface wave field for varying wave age: (left)  $\mathcal{R}_{uh_t}$ , and (right)  $\mathcal{R}_{uh}$ .  $C_p/U_a = 1.1$  (black), 1.3 (blue), 2.4 (green), and 4.2 (red). (right) The thin colored horizontal lines denote the nondimensional reference height  $\zeta_a/z_i$  above the water surface for that particular simulation.

boundary layer (MABL) coupled to a broadband time-dependent surface gravity wave field is described. The algorithm uses a coordinate transformation from physical to computational space that is wave following and accounts for the vertical motion of the mesh (or grid speed) in physical space: the time dependence of the grid and the grid speeds appear explicitly in the momentum and scalar time tendency and advection terms. The LES model is used to examine the wind-wave dynamics in a weakly unstable MABL for a range of geostrophic wind speeds  $U_g = 5, 10, 20,$  and  $25 \text{ m s}^{-1}$  with surface heat flux  $Q_* = 0.01 \text{ K m s}^{-1}$ . The broadband moving wave field is taken to be a wind-wave equilibrium spectrum with the significant wave height  $H_s = 6.4 \text{ m}$ . The wave age  $C_p/U_a = [1.1, 4.2]$  varies from near wind-wave equilibrium to a low-wind swell-dominated regime.

The high-resolution simulations show that near-surface wave-impacted turbulence smoothly blends into the bulk of the MABL over a vertical distance that depends on wave age. For low winds and strong swell

with wave age ( $C_p/U_a = 4.2$ ), wave signals can be found over an extended vertical distance. In this situation, wind speeds normalized by friction velocity computed at the standard reference height ( $\zeta_a = 10 \text{ m}$ ) are faster than their counterparts over a rough surface with no resolved waves. As the winds and waves approach equilibrium and the background turbulence increases, wave-induced signals are mainly generated by small-scale waves and their wave signatures are confined close to the water surface below  $\zeta_a$ . Wind profiles from Monin–Obukhov (MO) similarity formulas deviate from the LES wind profiles in the situation with large wave age. At wind-wave equilibrium, the agreement between LES and MO is good over a vertical range extending up to  $\zeta/z_i \sim 0.2$ . However, even at wind-wave equilibrium conditions, flow over moving waves differs from its counterpart over an identical but stationary wave spectrum. In the situation of stationary bumps, the wavy surface has a larger roughness parameter and the vertical height where the winds blend into a log-linear profile is higher.

A nearly-constant-flux layer for streamwise momentum extends up to  $\zeta_a$ ; the momentum flux budget computed in wave-following coordinates includes turbulent flux, pressure–wave slope correlations, and subgrid-scale contributions. A similar budget for spanwise momentum flux decreases by about 8% over  $0 < \zeta < \zeta_a$ . Below  $\zeta_a$  the momentum flux balance smoothly shifts between the turbulent flux, pressure–wave slope, and SGS contributions as the water surface is approached. At wind-wave equilibrium, the wave-induced form stress is negative and primarily confined close to the water surface while, at large wave age, wave-driven winds are produced by a positive form stress that extends well above  $\zeta_a$ . The cospectrum between surface pressure and wave slope, essentially the spectral content of the form stress, switches sign between positive and negative values at low wavenumbers ( $k_x < 0.4 \text{ m}^{-1}$ ) depending on wave age. At higher wavenumbers, the form stress is negative and small scales ( $\lambda < 15 \text{ m}$ ) contribute to the overall surface drag. This suggests that higher-resolution LESs are needed to evaluate the viscous and pressure contributions to surface drag at wind-wave equilibrium. The resolved velocity variances also exhibit wave-age dependence. Higher variances, especially for vertical velocity, are produced by wave pumping at large wave age.

Flow visualization and wind-wave correlations further illustrate the dependence on wave age. Vertical ( $w$ ) and streamwise ( $u$ ) velocity are best correlated with  $\partial h/\partial t$  and  $h$ , respectively; at large wave age, the correlations approach (1,  $-1$ ) at the water surface. At wind-wave equilibrium,  $w$  and  $u$  are only weakly correlated with wave height at  $\zeta_a$ . For the combination of weak surface heating and winds considered, depth-filling shear-convective rolls develop in the MABL and the entrainment flux at the top of the boundary layer depends strongly on wind speed. Large entrainment events extend from the inversion down to the middle of the MABL.

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Any opinions, findings, and conclusions or recommendations expressed in this publication are those of the author(s) and do not necessarily reflect the views of the National Science Foundation.

## APPENDIX

### Computation of Surface Fluxes

At every time step, surface fluxes are computed in a local wave-fitted Cartesian coordinate system  $\mathbf{x}'$  assuming law-of-the-wall formulas at all  $(x, y)$  or  $(\xi, \eta)$  surface points. These fluxes are converted into the LES Cartesian system  $\mathbf{x}$  so that they can be used as SGS surface fluxes in (9). The sequence of steps is as follows:

- 1) Build the base vectors parallel, perpendicular, and normal to the wave surface that define the local  $\mathbf{x}'$  coordinate system. Compute the surface wind, momentum, and temperature fluxes in the  $\mathbf{x}'$  system based on Monin–Obukhov (MO) similarity theory.
- 2) Build the matrix of direction cosines  $\mathbf{a}$  that transforms momentum fluxes from  $\mathbf{x}' \leftrightarrow \mathbf{x}$ .

#### a. Surface definition and surface wind

Given the  $(x, y, z)$  surface coordinates, the vectors aligned with the surface  $(\xi, \eta)$  gridlines for  $\zeta = 0$  are

$$\begin{aligned} \mathbf{t}_1 &= \mathbf{i} + \frac{\Delta z}{\Delta x} \mathbf{k} \quad (\text{constant } \eta), \\ \mathbf{t}_2 &= \mathbf{j} + \frac{\Delta z}{\Delta y} \mathbf{k} \quad (\text{constant } \xi), \end{aligned} \quad (\text{A1})$$

with  $\Delta x$ ,  $\Delta y$ , and  $\Delta z$  displacements taken along the surface gridlines, and  $\mathbf{i}$ ,  $\mathbf{j}$ , and  $\mathbf{k}$  are unit vectors. The surface normal is

$$\mathbf{n} = \mathbf{t}_1 \times \mathbf{t}_2, \quad (\text{A2})$$

and the unit base vectors are  $(\hat{\mathbf{t}}_1 = \mathbf{t}_1/|\mathbf{t}_1|, \hat{\mathbf{t}}_2 = \mathbf{t}_2/|\mathbf{t}_2|, \hat{\mathbf{n}} = \mathbf{n}/|\mathbf{n}|)$ .

In the LES, the Cartesian components of the wind vector at the first grid point off the surface are  $\mathbf{u} = u\mathbf{i} + v\mathbf{j} + w\mathbf{k}$ , and the velocity components of the water waves are  $\mathbf{u}_o = u_o\mathbf{i} + v_o\mathbf{j} + w_o\mathbf{k}$ . Following standard practice, we assume that the surface stress acts in a direction parallel to the surface wind and depends on the relative motion between the wind and water (e.g., Li 1995). The relative wind vector  $\mathbf{u}_s = \delta\mathbf{u} = \mathbf{u} - \mathbf{u}_o$  projected onto the surface is

$$\mathbf{u}_s = (\delta\mathbf{u} \cdot \mathbf{t}_1)\mathbf{t}_1 + (\delta\mathbf{u} \cdot \mathbf{t}_2)\mathbf{t}_2 = u_s^{(1)}\mathbf{t}_1 + u_s^{(2)}\mathbf{t}_2, \quad (\text{A3})$$

where  $u_s^{(1)}$  and  $u_s^{(2)}$  are relative surface wind components aligned with vectors  $\mathbf{t}_1$  and  $\mathbf{t}_2$ , respectively.



*b. Bulk transfer coefficients  $C_d$  and  $C_h$  at the water surface*

To compute fluxes at the water use the bulk aerodynamic formulas for momentum and heat:

$$\tau_o = -\hat{u}_*^2 = -C_d |\mathbf{u}_s|^2, \quad (\text{A4a})$$

$$Q_* = -C_h |\mathbf{u}_s| (\theta_s - \theta_{\text{surf}}). \quad (\text{A4b})$$

In the above,  $\tau_o$  is the magnitude of the surface stress;  $C_d$  and  $C_h$  are bulk transfer coefficients;  $\hat{u}_*$  is the surface friction velocity, which is not equal to the friction velocity  $u_{*a}$  at  $\zeta_a$ ;  $\theta_s$  is the potential temperature at the first grid point off the surface (i.e., at the same location as  $|\mathbf{u}_s|$ );  $\theta_{\text{surf}}$  is the temperature of the surface; and  $Q_*$  is the surface heat (temperature) flux. Under the assumption that the surface shear stress points in the direction of the unit base vector  $\hat{\mathbf{u}}_s$ :

$$\boldsymbol{\tau}' = \tau_o \hat{\mathbf{u}}_s = -C_d |\mathbf{u}_s|^2 \left( \frac{u_s^{(1)}}{|\mathbf{u}_s|} \hat{\mathbf{t}}_1 + \frac{u_s^{(2)}}{|\mathbf{u}_s|} \hat{\mathbf{t}}_2 \right), \quad (\text{A5})$$

or

$$\boldsymbol{\tau}' = -C_d |\mathbf{u}_s| (u_s^{(1)} \hat{\mathbf{t}}_1 + u_s^{(2)} \hat{\mathbf{t}}_2). \quad (\text{A6})$$

For a flat surface with  $(\Delta z/\Delta x, \Delta z/\Delta y) = 0$ , (A6) becomes

$$\boldsymbol{\tau}' = -C_d |\mathbf{u}_s| (u_s^{(1)} \mathbf{i} + u_s^{(2)} \mathbf{j}), \quad (\text{A7})$$

which is the variation in flat LES codes. In the  $\mathbf{x}'$  coordinate system, the surface momentum flux  $\boldsymbol{\tau}'$  is a symmetric matrix with two nonzero components.

In the absence of detailed information use MO similarity arguments as for a flat surface to compute transfer coefficients. Given the expressions

$$|\mathbf{u}_s| = \frac{\hat{u}_*}{\kappa} \left[ \ln \left( \frac{z_s}{z_o} \right) + \psi_m \left( \frac{z_s}{L} \right) \right], \quad (\text{A8a})$$

$$\theta_s - \theta_{\text{surf}} = -\frac{Q_*}{\hat{u}_* \kappa} \left[ \ln \left( \frac{z_s}{z_o} \right) + \psi_h \left( \frac{z_s}{L} \right) \right], \quad (\text{A8b})$$

where the von Kármán constant is  $\kappa$ , the surface roughness is  $z_o$ , the normal distance from the surface to the first grid point is  $z_s$ , and the MO length is  $L$ . The functions  $\psi_m$  and  $\psi_h$  are traditional MO similarity functions (e.g., Large et al. 1994). We use iteration to solve (A8a) and (A8b) for  $\hat{u}_*$  and  $\theta_{\text{surf}}$  when  $Q_*$  is given.

*c. Matrix of direction cosines  $[\mathbf{a}]$*

The matrix of direction cosines connects the  $\mathbf{x}'$  and  $\mathbf{x}$  coordinate systems:

$$\mathbf{x}' = \mathbf{a} \mathbf{x} \quad \text{where} \quad \mathbf{a} = [\hat{\mathbf{u}}_s, \hat{\mathbf{r}}, \hat{\mathbf{n}}]. \quad (\text{A9})$$

The terms  $\hat{\mathbf{u}}_s$ ,  $\hat{\mathbf{r}}$ , and  $\hat{\mathbf{n}}$  are unit base vectors with  $\hat{\mathbf{r}} = \hat{\mathbf{n}} \times \hat{\mathbf{u}}_s$ . Transformation of stress between two Cartesian coordinate systems obeys the rules for a second-order tensor [e.g., see p. 147 in Goldstein (1950)]:

$$\boldsymbol{\tau}' = \mathbf{a} \boldsymbol{\tau} \mathbf{a}^T \quad \text{or} \quad \mathbf{a}^T \boldsymbol{\tau}' \mathbf{a} = \boldsymbol{\tau}. \quad (\text{A10})$$

Expanding the matrix multiplications in (A10) and utilizing the properties of  $a_{ij}$ , the transformation of stress from the local wave-fitted Cartesian coordinate system to the LES coordinate system is

$$\boldsymbol{\tau} = \tau_o b_{ij} = \tau_o \begin{bmatrix} 2a_{11}a_{31} & a_{11}a_{32} + a_{31}a_{12} & a_{11}a_{33} + a_{13}a_{31} \\ a_{12}a_{31} + a_{11}a_{32} & 2a_{12}a_{32} & a_{12}a_{33} + a_{13}a_{32} \\ a_{11}a_{33} + a_{13}a_{31} & a_{13}a_{32} + a_{12}a_{33} & 2a_{13}a_{33} \end{bmatrix}. \quad (\text{A11})$$

The right-hand side of (A11) is a full symmetric matrix. If the surface is 2D [i.e., no variation in  $y$  (or  $\eta$ )], then the direction cosine of the  $\mathbf{j}$  component of the surface normal vector  $a_{32}$  is 0. Then (A11) reduces to a similar transformation matrix as described by Henn and Sykes (1999) [see (16) in their paper].

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